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Data Show That U.S. Wake-turbulence Accidents Are Most Frequent at Low Altitude and During Approach and Landing



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A340 Crew Conducts Takeoff From Airport Taxiway



The incident report says that the flight crew was cleared for takeoff on Runway 32; instead, they conducted the takeoff on a taxiway nearly perpendicular to the runway.

Cover photo: Dryden Flight Research Center, B-727 Vortex Study, U.S. National Aeronautics and Space Administration (NASA)

Flight Safety Foundation is an international membership organization dedicated to the continuous improvement of aviation safety. Nonprofit and independent, the Foundation was launched officially in 1947 in response to the aviation industry's need for a neutral clearinghouse to disseminate objective safety information, and for a credible and knowledgeable body that would identify threats to safety, analyze the problems and recommend practical solutions to them. Since its beginning, the Foundation has acted in the public interest to produce positive influence on aviation safety. Today, the Foundation provides leadership to more than 880 member organizations in more than 145 countries.

Data Show That U.S. Wake-turbulence Accidents Are Most Frequent at Low Altitude and During Approach and Landing

In wake-turbulence accidents and incidents from 1983 through 2000, about 10 percent of the aircraft weighed more than 30,000 pounds/13,600 kilograms, and two-thirds of the pilots held commercial pilot certificates or airline transport pilot certificates.

Patrick R. Veillette, Ph.D.

From January 1983 through December 2000, there were 130 aircraft accidents and 60 aircraft incidents in the United States involving wake turbulence (Figure 1; Figure 2, page 2).¹ Among these, there were 14 fatal accidents (11 percent of the total) and 20 serious-injury accidents (15 percent of the total). Thirty-five people were killed, 25 people were injured seriously, and 57 people received minor injuries; 36 of the accident aircraft were destroyed, and 76 accident aircraft received substantial damage.²

To identify trends involved in the accidents, the author conducted a study that included analysis of U.S. National Transportation Safety Board (NTSB) reports on the 130 accidents and U.S. Federal Aviation Administration (FAA) reports on the 60 incidents from 1983 through 2000. The study also included analysis of U.S. National Aeronautics and Space Administration (NASA) Aviation Safety Reporting System (ASRS)³ reports involving 165 aircraft that were flown into wake turbulence between January 1988 and December 1999 (see Appendix, page 33).

The study found that, of the 130 accidents in the NTSB database, the 60 incidents in the FAA database and the 165 events in the ASRS database:

Seventy-four accidents (57 percent), 41 incidents (68 percent) and 106 events (64 percent) occurred during the approach-and-landing phase of flight (Table 1, page 2; Table 2, page 3; Table 3, page 3).⁴ Twenty-four accidents



Figure 1

(18 percent), 13 incidents (22 percent) and 37 events (22 percent) occurred during the takeoff phase of flight;

- Eighty-seven accidents (67 percent), 47 incidents (78 percent) and 78 events (47 percent) occurred as a result of wake turbulence at and below 200 feet above ground level (AGL [Figure 3, page 4; Figure 4, page 5, Figure 5, page 5]);
- Wake-turbulence accidents and wake-turbulence incidents most frequently involved small aircraft that were flown



Figure 2

into the wake turbulence of other small aircraft — in 92 accidents (71 percent) and 37 incidents (62 percent). *In this study, except where noted otherwise, aircraft weight categories are those defined by ASRS. (ASRS weights in kilograms are rounded.)* Small aircraft are defined using ASRS criteria as weighing 5,000 pounds/2,300 kilograms or less (Table 4, page 6). Nevertheless, 13 accidents (10 percent) and nine incidents (15 percent) involved aircraft weighing more than 30,000 pounds/13,600 kilograms (Table 5, page 7; Table 6, page 8; see "Civil Aviation Authorities Use Different Weight Categories, Separation Requirements," page 9); and, • Eighty-six accidents (66 percent), 27 incidents (45 percent) and 110 events (67 percent) occurred during wind conditions of 10 knots or less (Figure 6, page 12; Figure 7, page 12; Figure 8, page 13).

Various Forms of Wake Turbulence Create Problems

Wake turbulence is defined by FAA as "phenomena resulting from the passage of an aircraft through the atmosphere."⁵ The term refers to several forms of wake turbulence, including wake vortices, which are defined by FAA as "circular patterns of air

| Phase o | f Flight o | f U.S. W | Table 1 ake-turbulence Acc | idents, 1983 [.] | -2000 | | | |
|----------------------|---|---|---|--|--|--|--|--|
| | Leading Aircraft | | | | | | | |
| Phase of Flight | Takeoff | Cruise | Approach and Landing | Maneuvering | Unspecified | Row Total | | |
| Takeoff | 19 | - | 2 | 2 | 1 | 24 | | |
| Cruise | - | 3 | 6 | _ | - | 9 | | |
| Approach and Landing | 7 | - | 64 | 2 | 1 | 74 | | |
| Maneuvering | - | _ | - | 23 | _ | 23 | | |
| Column Total | 26 | 3 | 72 | 27 | 2 | 130 | | |
| | Phase of Flight Takeoff Cruise Approach and Landing Maneuvering | Phase of FlightTakeoffTakeoff19Cruise-Approach and Landing7Maneuvering- | Phase of FlightTakeoffCruiseTakeoff19-Cruise-3Approach and Landing7-Maneuvering | Phase of Flight of U.S. Wake-turbulence Acc Leading AircraftPhase of FlightTakeoffCruiseApproach and LandingTakeoff19-2Cruise-36Approach and Landing7-64Maneuvering | Phase of Flight of U.S. Wake-turbulence Accidents, 1983Leading AircraftPhase of FlightTakeoffCruiseApproach and LandingManeuveringTakeoff19-22Cruise-36-Approach and Landing7-642Maneuvering2323 | Phase of Flight of U.S. Wake-turbulence Accidents, 1983–2000Leading AircraftPhase of FlightTakeoffCruiseApproach and LandingManeuveringUnspecifiedTakeoff19-221Cruise-36Approach and Landing7-6421Maneuvering23_ | | |

Table 2Phase of Flight of U.S. Wake-turbulence Incidents, 1983–2000

| | Leading Aircraft | | | | | | | |
|---------|------------------|--------------------------|--|---|---|--|--|--|
| Takeoff | Cruise | Approach and Landing | Maneuvering | Unspecified | Row Total | | | |
| 5 | - | - | - | 8 | 13 | | | |
| - | 4 | - | - | 1 | 5 | | | |
| 6 | - | 16 | - | 19 | 41 | | | |
| - | - | _ | 1 | _ | 1 | | | |
| 11 | 4 | 16 | 1 | 28 | 60 | | | |
| | 5 6 | 5 – – 4 6 – – – | TakeoffCruiseApproach and Landing54-6-16 | TakeoffCruiseApproach and LandingManeuvering546-161 | TakeoffCruiseApproach and LandingManeuveringUnspecified58-416-16-191_ | | | |

Source: Patrick R. Veillette, Ph.D., from U.S. Federal Aviation Administration data on 60 incidents

| Table 3 | |
|---|--|
| Phase of Flight of U.S. Wake-turbulence Events, 1988–1999 | |

| Maneuvering | Row Total |
|-------------|-----------|
| 0 | 37 |
| 0 | 22 |
| 0 | 106 |
| 0 | 0 |
| 0 | 165 |
| _ | 0 |

Source: Patrick R. Veillette, Ph.D., from U.S. National Aeronautics and Space Administration Aviation Safety Reporting System data on 165 events

created by the movement of an airfoil through the air when generating lift."⁶Other forms of wake turbulence include thruststream turbulence (jet blast), propeller wash and rotor wash (see "Data Show That 13 U.S. Accidents From 1983–2000 Involved Helicopter Wake Turbulence," page 15).

All aircraft generate wake vortices, but the intensity of the wake vortices generated by a specific aircraft is determined by many factors, including the aircraft's weight, speed, wingspan (or rotorblade design), and the atmospheric conditions in which the aircraft is being flown (see "Atmospheric Conditions, Aircraft Characteristics Determine Intensity of Wake Vortices," page 19). Wake vortices are generated in part by the same forces that provide lift to the airplane. High-pressure air from the lower surface of the wing flows around the wing tip into low-pressure air above the wing. The result is a pair of wake vortices that rotate from the wings in opposite directions — as viewed from behind the airplane, the right-wing vortex rotates clockwise — creating an area of turbulence behind the airplane. (Some airplanes, especially those with multiple flaps and cutouts [gaps] between the flaps, initially produce multiple vortices, which quickly combine into one vortex for each wing.)

Typically, a vortex develops a circular motion around a core region. The core varies in size from several inches in diameter to several feet in diameter. The speed of the air movement within the core can be more than 300 feet (92 meters) per second. The core is surrounded by an outer region of the vortex, as large as 100 feet (31 meters) in diameter, with air moving at speeds that decrease as the distance from the core increases.⁷ The wake vortices can extend as far as 10 nautical miles (19 kilometers) behind a large aircraft, typically descending for about 30 seconds at a rate of about 300 feet per minute to 500 feet per minute. The descent rate typically slows to near zero between 500 feet and 900 feet below the aircraft's flight path. Wake vortices can persist as long as three minutes, depending on various factors, including wind conditions.⁸

The typical risk to an aircraft flown into wake turbulence is an induced roll, in which the intensity of the vortices forces the aircraft to roll. In some occurrences, an induced roll can exceed





the roll-control authority of the aircraft. Flight into wake turbulence sometimes causes in-flight structural damage to aircraft and fatal injuries to occupants.

More Than Half of Wake-turbulence Accidents Occur During Approach and Landing

Data show that wake-turbulence accidents, incidents and events were more frequent during approach and landing than during any other phase of flight. Of the 130 wake-turbulence accidents in the NTSB database, 74 accidents (57 percent) occurred during approach and landing; in 64 of those accidents (86 percent), the leading aircraft (the aircraft that generated the wake turbulence) also was in the approach-and-landing phase.

In 16 of the 41 approach-and-landing incidents (39 percent) in the FAA database and 92 of the 106 approach-and-landing events (87 percent) in the ASRS database, the leading aircraft also was in the approach-and-landing phase.

Of the 130 wake-turbulence accidents, 24 accidents (18 percent) occurred during takeoff; the leading aircraft also was in the takeoff phase of flight in 19 of the 24 accidents (79 percent). Of the 60 incidents, 13 incidents (22 percent) occurred during takeoff; the leading aircraft also was in the takeoff phase of flight in five of the 13 incidents (38 percent.) Thirty-seven (22 percent) of the 165 events occurred during takeoff; of the 37 events, 30 events (81 percent) involved leading aircraft that were in the takeoff phase or were in the initial-climb phase of flight.

Because wake vortices move with the wind, and aircraft typically take off or land into the wind, wake vortices often drift toward other aircraft at the departure end of the runway or on final approach. Studies by the U.S. Air Force and NASA have found that a trailing aircraft can avoid wake turbulence by lifting off 3,000 feet before the rotation point of the leading aircraft.⁹ The studies said that lighter aircraft should remain upwind of larger aircraft and above their flight paths — a recommendation similar to that contained in the FAA *Aeronautical Information Manual (AIM)*.¹⁰

Although the recommendation to fly an aircraft above the leading aircraft's flight path to avoid wake turbulence may have been effective in the past, because of the increased climb performance of the current generation of transport aircraft, many trailing aircraft do not have sufficient performance to fly above the flight path of a high thrust-to-weight-ratio transport airplane.¹¹

Of the 130 accidents in the NTSB database, 23 accidents (18 percent) occurred during maneuvering — a category that includes such diverse activities as conducting stall-recovery procedures in a practice area, conducting 360-degree turns for spacing and conducting agricultural-application flights. In each accident, the leading aircraft also was maneuvering. Most of these accidents involved aircraft conducting agricultural operations, and some involved aircraft that were flown into their own wake turbulence.

Of the 130 accidents, nine accidents (7 percent) occurred during the cruise phase of flight. Of the 60 incidents, five



Figure 4



Figure 5

incidents (8 percent) occurred during cruise. Of the 165 events, 22 of them (13 percent) occurred during cruise.

Because their duties require movement in the cabin, flight attendants are particularly vulnerable to the effects of

unexpected flight into wake turbulence. Each of the accidents and incidents that occurred during cruise flight resulted in injuries to flight attendants; some occurrences also resulted in injuries to passengers. Four accidents resulted in serious injuries to a total of four flight attendants; five

Table 4Aircraft Categories Used by NASA ASRS

| Aircraft Category | Weight in Pounds | Weight in Kilograms |
|---------------------------|---------------------|------------------------|
| Small | 5,000 or less | 2,300 or less |
| Small Transport | 5,001 to 14,500 | 2,300 to 6,600 |
| Light Transport | 14,501 to 30,000 | 6,600 to 13,600 |
| Medium Transport | 30,001 to 60,000 | 13,600 to 27,200 |
| Medium-large Transport | 60,001 to 150,000 | 27,200 to 68,000 |
| Large Transport | 150,001 to 300,000 | 68,000 to 136,000 |
| Heavy Transport | more than 300,000 | more than 136,000 |

Note: Figures in kilograms have been rounded.

Source: U.S. National Aeronautics and Space Administration (NASA) Aviation Safety Reporting System (ASRS)

accidents and five incidents caused minor injuries to 10 flight attendants, and three accidents caused minor injuries to 14 passengers. The accident/incident reports did not say how the passengers were injured or whether they were wearing seat belts.

Wake vortices sometimes persist longer at high altitudes than at lower altitudes. This can be attributed to two factors:

- Because aircraft are in the clean configuration (with landing gear and flaps retracted) during cruise flight, they generally generate more coherent but weaker wake vortices during cruise than during other phases of flight. (Coherent vortices are generated by smooth wing surfaces, uninterrupted by the presence of multiple flaps and cutouts between sections of flaps. These smooth surfaces generate one large vortex, instead of the multiple vortices that initially are generated by wing surfaces with multiple flaps and that quickly combine into one larger vortex from each wing.); and,
- Atmospheric turbulence, which helps dissipate wake vortices, typically is not as prevalent at higher cruise altitudes. Therefore, the absence of atmospheric turbulence also results in an environment that enables wake vortices to remain coherent and to persist for longer periods of time.^{12,13}

Winds, Atmospheric Turbulence Influence Wake-vortex Development

Wake-turbulence accidents, incidents and ASRS events occurred in varying wind conditions, but data showed that most occurred when winds were between three knots and 10 knots. (Data on wind conditions were not available in all reports.) Of the 130 accidents in the NTSB database, 79 accidents (61 percent) occurred when winds were between three knots and 10 knots (Figure 6). Of the 60 incidents in the FAA database, 26 incidents (43 percent) occurred in winds between three knots and 10 knots (Figure 7). Of the 165 events in the ASRS database, 99 events (60 percent) occurred in winds between three knots and 10 knots (Figure 8).

The speed and direction of the wind determine the horizontal motion of the wake vortices. When wake vortices are formed near the ground or descend toward the ground, wind speed and wind direction influence the effects of vortices on landing aircraft and departing aircraft. If the wind is calm or is moving along the runway heading, a pair of vortices moves apart and away from the flight path of a landing aircraft or departing aircraft. With a crosswind of one knot to five knots, the lateral movement of the upwind vortex slows and the lateral movement of the downwind vortex increases; as a result, the upwind vortex can remain near the flight path, and the downwind vortex can move more quickly toward another runway. With a cross the flight path.¹⁴

A tail wind can move the vortices of a leading aircraft forward into the touchdown zone. The *AIM* says that a light quartering tail wind requires "maximum caution" and that pilots must be aware of large aircraft upwind from their approach flight paths and takeoff flight paths and take appropriate action to avoid wake turbulence.¹⁵

Of the 130 accidents in the NTSB database, 16 accidents (12 percent) occurred on or near closely spaced parallel runways when winds were less than eight knots, as did four (7 percent) of the 60 incidents in the FAA database and 28 (17 percent) of the 165 events in the ASRS database.

A study of the cross-runway movement of wake vortices at Frankfurt (Germany) Airport, where parallel runways are used frequently, found that under stable atmospheric conditions, wake vortices could persist up to 3.5 minutes and could travel about 1,641 feet (500 meters) perpendicular to the runway when influenced by crosswinds of six knots to eight knots, measured about 33 feet AGL.¹⁶

Other research found that:

- In crosswinds of 15 knots or more, a vortex may exhibit significant rotational speed even after moving 2,500 feet (763 meters);^{17,18}
- A downwind vortex from a Boeing 757 has sufficient force after 87 seconds to upset a McDonnell Douglas DC-9 on a closely spaced parallel runway;¹⁹ and,
- Downwind vortices typically ascend while moving downwind, which places the vortices at higher altitudes than most pilots expect.²⁰

Table 5Weight Categories of Trailing Aircraft and Leading (Wake-generating)Aircraft in U.S. Wake-turbulence Accidents, 1983–2000

| | | | Leading Aircraft | | | | | | | |
|----------|-------------------------------|--------------------|---------------------------------|---------------------------------|----------------------|----------------------------|---------------------------------|---------------------------------|-------------|--------------|
| | Categories | Small ¹ | Small Transport ² | Light Transport ³ | Medium Transport⁴ | Medium-large Transport⁵ | Large Transport ⁶ | Heavy Transport ⁷ | Unspecified | Row Total |
| | Small ¹ | 29 | 14(1F) | 6 | 6(1F) | 15(4F) | 12(4F) | 4 | 6 | 92 |
| Ħ | Small Transport ² | - | 4 | 1 | 2(1F) | 4(1F) | 1 | 7(1F) | 2 | 21 |
| Aircraft | Light Transport ³ | - | - | - | - | 1 | 2(2F) | 1 | - | 4 |
| - | Medium Transport ⁴ | - | - | - | 1 | 2 | - | 3 | - | 6 |
| Trailing | Medium-large Transport⁵ | _ | _ | _ | _ | 1 | 2 | 3 | - | 6 |
| F | Large Transport ⁶ | - | - | - | - | - | - | - | - | 0 |
| | Heavy Transport ⁷ | - | - | - | - | - | - | 1 | - | 1 |
| | Column Total | 29 | 18 | 7 | 9 | 23 | 17 | 19 | 8 | 130 |

Notes: The number of fatal accidents (F) is shown in parentheses. Numbers in kilograms have been rounded.

¹ U.S. National Aeronautics and Space Administration (NASA) Aviation Safety Reporting System (ASRS) defines small aircraft as weighing 5,000 pounds/2,300 kilograms or less.

² NASA ASRS defines small transport aircraft as weighing 5,001 pounds/2,300 kilograms to 14,500 pounds/6,600 kilograms.

³ NASA ASRS defines light transport aircraft as weighing 14,501 pounds/6,600 kilograms to 30,000 pounds/13,600 kilograms.

⁴ NASA ASRS defines medium transport aircraft as weighing 30,001 pounds/13,600 kilograms to 60,000 pounds/27,200 kilograms.

⁵ NASA ASRS defines medium-large transport aircraft as weighing 60,001 pounds/27,200 kilograms to 150,000 pounds/68,000 kilograms.

⁶ NASA ASRS defines large transport aircraft as weighing 150,001 pounds/68,000 kilograms to 300,000 pounds/136,000 kilograms.

⁷ NASA ASRS defines heavy transport aircraft as weighing more than 300,000 pounds/136,000 kilograms.

Source: Patrick R. Veillette, Ph.D., from U.S. National Transportation Safety Board data on 130 accidents

Most Wake-turbulence Accidents Occur Near Runway Threshold

Of the 130 accidents in the NTSB database, 87 accidents (67 percent) occurred at or below 200 feet AGL (Figure 3). Of the 60 incidents in the FAA database, 47 incidents (78 percent) occurred at and below 200 feet AGL (Figure 4). Of the 165 events in the ASRS database, 78 events (47 percent) occurred at and below 200 feet AGL (Figure 5).

Similar findings resulted from an earlier study of data gathered by the U.K. Civil Aviation Authority (CAA) Wake Vortex Reporting Program (WVRP), involving 515 wake-turbulence occurrences in the United Kingdom from 1982 through 1990. The study found that most wake-turbulence occurrences were 100 feet to 200 feet above the runway threshold; the next-mostfrequent altitude for wake-turbulence occurrences was between 2,000 feet AGL and 4,000 feet AGL (where aircraft typically level off during instrument landing system [ILS] approaches).²¹

A simulator-based study of nine Learjet pilots was conducted in 1977 to determine their criteria for assessing the risks of a wake-vortex occurrence and aircraft response. The pilots said that the maximum acceptable vortex-induced bank angle depended on the altitude of the occurrence and whether the flight was in visual meteorological conditions (VMC) or instrument meteorological conditions (IMC).²²

The Learjet pilots' primary criteria for rating an occurrence as hazardous were altitude at the time of the occurrence and the amount of altitude lost as a result of the occurrence. The pilots' ratings of risk became more consistent as altitude decreased. The study participants based their judgments on the lack of time and/or altitude to safely recover the aircraft from the vortex-induced motion.

The pilots said that in VMC at 100 feet AGL, the maximum acceptable induced bank angle was six degrees to eight degrees. The pilots said that in VMC at 500 feet AGL, the maximum acceptable induced bank angle was 20 degrees to 25 degrees. Responses varied among the study's participants because of their experience in different aircraft types.

The pilots said that in IMC, seven degrees was the maximum induced bank angle considered acceptable at a breakout altitude (altitude of transition from instrument references to

Table 6Weight Categories of Trailing Aircraft and Leading (Wake-generating)Aircraft in U.S. Wake-turbulence Incidents, 1983–2000

| | | | Leading Aircraft | | | | | | | |
|----------|-------------------------------|--------------------|---------------------------------|---------------------------------|----------------------|----------------------------|---------------------------------|---------------------------------|-------------|--------------|
| | Categories | Small ¹ | Small Transport ² | Light Transport ³ | Medium Transport⁴ | Medium-large Transport⁵ | Large Transport ⁶ | Heavy Transport ⁷ | Unspecified | Row Total |
| | Small ¹ | 4 | 3 | 2 | 3 | 2 | 1 | 1 | 21 | 37 |
| raft | Small Transport ² | - | - | - | - | 4 | 1 | - | 4 | 9 |
| Aircra | Light Transport ³ | - | - | - | - | 1 | - | 1 | 3 | 5 |
| | Medium Transport ⁴ | - | - | - | - | _ | 2 | 1 | 1 | 4 |
| Trailing | Medium-large Transport⁵ | _ | _ | _ | _ | _ | _ | 2 | 2 | 4 |
| - | Large Transport ⁶ | - | - | - | - | - | - | 1 | - | 1 |
| | Heavy Transport ⁷ | - | - | - | - | - | - | - | - | 0 |
| | Column Total | 4 | 3 | 2 | 3 | 7 | 4 | 6 | 31 | 60 |

Note: Numbers in kilograms have been rounded.

¹ U.S. National Aeronautics and Space Administration (NASA) Aviation Safety Reporting System (ASRS) defines small aircraft as weighing 5,000 pounds/2,300 kilograms or less.

² NASA ASRS defines small transport aircraft as weighing 5,001 pounds/2,300 kilograms to 14,500 pounds/6,600 kilograms.

³ NASA ASRS defines light transport aircraft as weighing 14,501 pounds/6,600 kilograms to 30,000 pounds/13,600 kilograms.

⁴ NASA ASRS defines medium transport aircraft as weighing 30,001 pounds/13,600 kilograms to 60,000 pounds/27,200 kilograms.

⁵ NASA ASRS defines medium-large transport aircraft as weighing 60,001 pounds/27,200 kilograms to 150,000 pounds/68,000 kilograms.

⁶ NASA ASRS defines large transport aircraft as weighing 150,001 pounds/68,000 kilograms to 300,000 pounds/136,000 kilograms.

⁷ NASA ASRS defines heavy transport aircraft as weighing more than 300,000 pounds/136,000 kilograms.

Source: Patrick R. Veillette, Ph.D., from U.S. Federal Aviation Administration data on 60 incidents

visual references) of 200 feet AGL. For altitudes above 350 feet AGL in IMC, the pilots said that a 10-degree bank angle induced by a wake vortex was the maximum bank angle for acceptable risk.²³

In the following ASRS report, the first officer of a Boeing 737-300 described his airplane's flight into wake turbulence — and the resulting vortex-induced roll of 15 degrees — just after takeoff in VMC behind an Airbus A320:

[The airplane] encountered severe wake turbulence at 200 feet AGL on takeoff behind an Airbus. ... There was normal takeoff spacing behind this non-heavy aircraft. At 200 feet, we encountered wake [turbulence] that required full right aileron to counter. Even though total roll ... was only approximately 15 degrees to the left, the acceleration we felt was very pronounced. Without immediate aileron input, the roll to the left would have been much more severe. ... The experience made me a firm believer that it doesn't take a "heavy" to cause severe wake turbulence if you hit it just right.²⁴ Some aircraft can tolerate a smaller bank angle at touchdown than others. For example, a Boeing 727 can tolerate only a 12-degree bank angle when touching down in a normal flare. Any bank angle greater than 12 degrees causes the outboard sections of the flaps (which, because of the aircraft's design, are close to the ground during takeoff and landing) to strike the ground. If the aircraft is descending at a slightly faster sink rate upon touchdown, a 7.5-degree bank angle can result in the outboard sections of flaps striking the ground. This is primarily a result of the higher nose-up pitch attitude associated with a faster sink rate.²⁵

More Than 25 Percent of Wake-turbulence Events Occur at Major Metropolitan Airports

Data from the 165 events in the ASRS database showed that flight into wake turbulence occurred at various types of airports.

Of the 165 events, 26 events (16 percent) occurred at airports used primarily as major hubs for air carrier traffic; light

Civil Aviation Authorities Use Different Weight Categories, Separation Requirements

The International Civil Aviation Organization (ICAO) has developed standards for aircraft wake-turbulence separation minimums based on a system that groups aircraft into three categories according to weight (Table 1).

Table 1International Civil Aviation Organization(ICAO) Recommended MinimumWake-turbulence Separation Distances1

| Leading Aircraft | Trailing Aircraft | Minimum Separation Distance |
|---------------------|----------------------|--------------------------------------|
| Heavy ² | Heavy | 7.4 kilometers (4.0 nautical miles) |
| Heavy | Medium ³ | 9.3 kilometers (5.0 nautical miles) |
| Heavy | Light⁴ | 11.1 kilometers (6.0 nautical miles) |
| Medium | Light | 9.3 kilometers |

Note: Numbers in pounds have been rounded.

¹These wake-turbulence radar separation minimums apply to aircraft during the approach phase and the departure phase when the aircraft is operating behind another aircraft at the same altitude or less than 1,000 feet below that aircraft, when both aircraft are using the same runway or parallel runways separated by less than 760 meters (2,494 feet) or when an aircraft is crossing behind another aircraft at the same altitude or less than 1,000 feet below that aircraft at the same altitude or less than 1,000 feet below that aircraft. Non-radar separation minimums include the following: for timed approaches, a two-minute separation for a medium aircraft behind a heavy aircraft, and a three-minute separation for a light aircraft behind a heavy aircraft or a medium aircraft; for departing aircraft in most situations, a minimum separation of two minutes between a light aircraft or a medium aircraft taking off behind a heavy aircraft and between a light aircraft taking off behind a medium aircraft.

²ICAO defines a heavy aircraft as weighing 136,000 kilograms/ 300,000 pounds or more.

³ICAO defines a medium aircraft as weighing less than 136,000 kilograms and more than 7,000 kilograms/15,000 pounds.

⁴ICAO defines a light aircraft as weighing 7,000 kilograms or less.

Source: International Civil Aviation Organization

The U.K. Civil Aviation Authority (CAA; Table 2) and the U.S. Federal Aviation Administration (FAA; Table 3, page 10) are among the authorities that have modified their definitions of aircraft weight categories and their separation minimums in the past 20 years following separate analyses of waketurbulence occurrence data.

(The three sets of definitions differ from those used for datagathering and analysis purposes by the U.S. National Aeronautics and Space Administration Aviation Safety Reporting System¹[Table 4, page 6].)

CAA established the Wake Vortex Reporting Program (WVRP), a voluntary reporting system, in 1972 to gather data on wake-turbulence occurrences.² In 1982, citing WVRP data, CAA changed its aircraft-weight categories from three categories to four categories to require greater separation distances for some types of aircraft that data showed may be more vulnerable to upset by wake turbulence when following heavy aircraft.³

Table 2 U.K. Civil Aviation Authority (CAA) Minimum Wake-turbulence Separation Distances¹

| Leading Aircraft | Trailing Aircraft | Minimum Separation Distance |
|---------------------|----------------------|--------------------------------------|
| Heavy ² | Heavy | 4.0 nautical miles (7.4 kilometers) |
| Heavy | Medium ³ | 5.0 nautical miles (9.3 kilometers) |
| Heavy | Small⁴ | 6.0 nautical miles (11.1 kilometers) |
| Heavy | Light⁵ | 8.0 nautical miles (14.8 kilometers) |
| Medium ⁶ | Medium | 3.0 nautical miles (5.6 kilometers) |
| Medium | Small | 4.0 nautical miles |
| Medium | Light | 6.0 nautical miles |
| Small | Medium or Small | 3.0 nautical miles |
| Small | Light | 4.0 nautical miles |

Note: Numbers in pounds have been rounded.

¹These minimum separation distances apply to aircraft on final approach. For aircraft departing from the same takeoff position on the same runway or departing from parallel runways less than 760 meters (2,494 feet) apart, a minimum separation of two minutes is required for medium aircraft, small aircraft or light aircraft following heavy aircraft and for light aircraft following medium aircraft or small aircraft.

²U.K. CAA defines a heavy aircraft as weighing 136,000 kilograms/300,000 pounds or more.

³U.K. CAA defines a medium aircraft as weighing more than 40,000 kilograms/90,000 pounds and less than136,000 kilograms.

⁴U.K. CAA defines a small aircraft as weighing more than 17,000 kilograms/37,500 pounds and less than 40,000 kilograms.

 $^5\text{U.K.}$ CAA defines a light aircraft as weighing 17,000 kilograms or less.

⁶When the leading medium aircraft is a Boeing 757, McDonnell Douglas DC-8, Boeing 707, Ilyushin II-62 or BAE Systems VC10, the minimum separation distance is four nautical miles.

Source: U.K. Civil Aviation Authority

An analysis of wake-turbulence incidents reported to CAA between 1972 and 1990 found that "[Boeing] 747 and [Boeing] 757 airplanes appear to produce significantly higher incident rates than the other airplanes considered, indicating ... that they produce stronger and more persistent vortices than the other aircraft in their respective weight categories. ... The cause of the higher B-757 incident rates is uncertain," said CAA. (The B-757 is the largest airplane in its CAA category — medium.) The analysis showed that the trailing aircraft most often affected by wake turbulence from the B-747 and B-757 were the McDonnell Douglas DC-9, the British Aircraft Corp. BAC 1-11 and the B-737.⁴

In the United States, FAA imposed no wake-turbulence aircraft-separation standards before the early 1970s. Instead, air traffic control (ATC) radar operating limits and, to a lesser extent, runway-occupancy restrictions dictated separation standards. In 1972, however, after an accident involving a Delta Air Lines DC-9-14 at Fort Worth, Texas, U.S., the U.S. National Transportation Safety Board said that FAA should

Table 3 U.S. Federal Aviation Administration (FAA) Minimum Wake-turbulence Separation Distances

Minimum **Separation Distance** Leading Trailing Aircraft Aircraft (before 1994) (1994 and later)1 Heavy² 4.0 nautical miles 4.0 nautical miles3 Heavv (7.4 kilometers) Heavy Large⁴ 5.0 nautical miles 5.0 nautical miles3 (9.3 kilometers) 5.0 nautical miles3 Heavy Small⁵ 6.0 nautical miles 6.0 nautical miles6 (11.1 kilometers) NA Large Large 3.0 nautical miles (5.6 kilometers) Large Small 4.0 nautical miles 4.0 nautical miles6 B-7577 4.0 nautical miles3 Heavy NA B-7577 Large NA 4.0 nautical miles3 B-7577 Small NA 5.0 nautical miles³ 5.0 nautical miles6

Note: Numbers in kilograms have been rounded.

¹Time or distance intervals are provided for aircraft departing behind a heavy aircraft or a B-757: either two minutes or the appropriate minimum separation distance of four nautical miles or five nautical miles.

²Before 1994, FAA defined a heavy aircraft as weighing more than 300,000 pounds/136,000 kilograms. The definition was changed in 1994 to include aircraft weighing more than 255,000 pounds/115,600 kilograms.

³Applies when the trailing aircraft is at the same altitude or less than 1,000 feet below the leading aircraft.

⁴Before 1994, FAA defined a large aircraft as weighing 12,500 pounds/5,670 kilograms to 300,000 pounds. The definition was changed in 1994 to include aircraft weighing more than 41,000 pounds/18,600 kilograms to 255,000 pounds.

⁵Before 1994, FAA defined a small aircraft as weighing less than 12,500 pounds. The definition was changed in 1994 to include aircraft weighing 41,000 pounds or less.

⁶Distance from the landing threshold after landing by the specified type of larger aircraft.

⁷FAA established a separate category for Boeing 757 aircraft in 1994, after a series of accidents and incidents involving aircraft that were flown behind B-757s during visual approaches to landing.

Source: U.S. Federal Aviation Administration

"re-evaluate wake-turbulence separation criteria for aircraft operating behind heavy jet aircraft" and should develop new ATC separation standards that considered the effects of wake turbulence on trailing aircraft.

(In that accident on May 30, 1972, the DC-9 was flown into the wake turbulence of a McDonnell Douglas DC-10 that had been 2.25 nautical miles (4.17 kilometers) ahead on the approach. The DC-9 struck the ground and was destroyed; the airplane's four occupants were killed.)⁵

After conducting flight tests in the early 1970s to determine wake-turbulence characteristics of jet aircraft, FAA established wake-turbulence aircraft separation criteria by categorizing aircraft, based upon their maximum takeoff weight, as heavy (more than 300,000 pounds/136,000 kilograms), large (more than 12,500 pounds/5,670 kilograms to 300,000 pounds) and small (12,500 pounds or less).

Those criteria were used until the early 1990s, when a series of accidents and incidents occurred involving aircraft that were being flown behind B-757s during visual approaches to landing. In December 1993, FAA issued a notice requiring specific wake-turbulence advisories to be issued by ATC to the crews of aircraft being flown behind heavy jets or B-757s.⁶ FAA also issued a bulletin cautioning pilots about the possibility of wake turbulence, especially when following a heavy jet or a B-757.⁷

In 1994, FAA modified the weight categories for purposes of wake-turbulence separation and established separate wake-turbulence separation criteria for aircraft following B-757s. The weight categories, still in effect, are for heavy aircraft (capable of takeoff weights of more than 255,000 pounds/115,600 kilograms), large aircraft (with maximum certificated takeoff weights of more than 41,000 pounds/18,600 kilograms to 255,000 pounds) and small aircraft (with maximum certificated takeoff weights of 41,000 pounds or less).⁸

Current procedures in Order 7110.65N, *Air Traffic Control,* require controllers to take various actions to help pilots avoid wake turbulence, including the following:

- To "issue wake turbulence cautionary advisories and the position, altitude if known, and direction of flight of the heavy jet or B-757" to pilots of visual flight rules (VFR) aircraft and pilots of instrument flight rules (IFR) aircraft who have accepted a visual approach or visual separation. Similar cautionary advisories are to be issued to the pilots of small aircraft following large aircraft;
- To issue similar advisories to pilots of aircraft being landed on the same runway or a parallel runway less than 2,500 feet (763 meters) away behind a heavy jet or a B-757 or to pilots of small aircraft being landed behind large aircraft;
- To separate aircraft on departure behind a heavy jet or B-757 by two minutes (i.e., a takeoff clearance should be issued two minutes after the beginning of a takeoff roll by a heavy jet or B-757); and,
- To issue cautionary information to pilots of "any aircraft if, in your opinion, wake turbulence may have an adverse effect on it. When traffic is known to be a heavy aircraft, include the word 'heavy' in the description."⁹

In the *Procedures for Air Navigation Services* — *Rules of the Air and Air Traffic Services,* ICAO provides procedures for wake-turbulence avoidance, including the following:

- Pilots should use the word "heavy" after the aircraft call sign in their first radio communication with ATC;
- Wake-turbulence radar separation minimums should apply when an aircraft is operating behind another aircraft at the same altitude or less than 1,000 feet below

the other aircraft, when both aircraft are using the same runway or parallel runways separated by less than 2,494 feet (760 meters) or when an aircraft is crossing behind another aircraft at the same altitude or less than 1,000 feet below the aircraft; and,

 Non-radar wake-turbulence separation minimums should provide for medium aircraft to follow heavy aircraft by two minutes in timed approaches and for light aircraft to follow heavy aircraft and medium aircraft by three minutes. During takeoffs from the same runway, from parallel runways separated by less than 2,494 feet or from other parallel runways or crossing runways if the trailing aircraft will cross the projected flight path of the leading aircraft at the same altitude or less than 1,000 feet below, a two-minute separation should be imposed (in most situations) for light aircraft and medium aircraft behind heavy aircraft and for light aircraft behind medium aircraft.¹⁰♦

- Patrick R. Veillette, Ph.D.

Notes

 The U.S. National Aeronautics and Space Administration (NASA) Aviation Safety Reporting System (ASRS) is a confidential incident-reporting system. The ASRS Program Overview said, "Pilots, air traffic controllers, flight attendants, mechanics, ground personnel and others involved in aviation operations submit reports to the ASRS when they are involved in, or observe, an incident or situation in which aviation safety was compromised. ... ASRS de-identifies reports before entering them into the incident database. All personal and organizational names are removed. Dates, times and related information, which could be used to infer an identity, are either generalized or eliminated."

ASRS acknowledges that its data have certain limitations. ASRS *Directline* (December 1998) said, "Reporters to ASRS may introduce biases that result from a greater tendency to report serious events than minor ones; from organizational and geographic influences; and from many other factors. All of these potential influences reduce the confidence that can be attached to statistical findings based on ASRS data. However, the proportions of consistently reported incidents to ASRS, such as altitude deviations, have been remarkably stable over many years. Therefore,

transport aircraft (defined by ASRS as those weighing 14,501 pounds/6,600 kilograms to 30,000 pounds) were the trailing aircraft in 21 of these events. Twenty-one events (13 percent) occurred in airspace surrounding major hub airports; light transport aircraft were involved in seven of these events, and general aviation aircraft (small aircraft) were involved in 14 events.

Analysis of events also showed that:

users of ASRS may presume that incident reports drawn from a time interval of several or more years will reflect patterns that are broadly representative of the total universe of aviation-safety incidents of that type."

- 2. The U.K. Civil Aviation Authority Wake Vortex Reporting Program (WVRP) was established to receive and review data on wake-turbulence occurrences. A report of a waketurbulence occurrence typically is submitted by the crew of the aircraft involved or by air traffic control (ATC), although formal procedures for reporting wake-turbulence occurrences by ATC exist only at London City Airport and Heathrow Airport. Additional data are collected from pilots of the aircraft that generated wake turbulence; the Meteorological Office; London Air Traffic Control Center, which provides recorded radar data; and airlines, which provide flight data recorder data. The data are analyzed to determine if the cause of each reported occurrence was, in fact, wake turbulence. WVRP was transferred in 1989 to the Air Traffic Control Evaluation Unit.
- Critchley, J.B.; Foot, P.B. "U.K. CAA Wake Vortex Database: Analysis of Incidents Reported Between 1972– 1990." In *Proceedings of the Aircraft Wake Vortices Conference*, Washington, D.C., U.S. Oct. 29–31, 1991.
- 4. Ibid.
- 5. U.S. National Transportation Safety Board. Aircraft Accident Report: Delta Air Lines, Inc. McDonnell Douglas DC-9-14, N3305L, Greater Southwest International Airport, Fort Worth Texas, May 30, 1972. NTSB-AAR-73-3.
- U.S. Federal Aviation Administration (FAA). FAA General Notice Issued on December 22, 1993. (Cited and reprinted in NTSB. Special Investigation Report: Safety Issues Related to Wake Vortex Encounters During Visual Approach to Landing. NTSB/SIR-94-01. Washington, D.C., U.S. 1994.)
- 7. FAA. *Wake Turbulence Accident Prevention Program* FSAT 93-38 and FSGA 93-15. Dec. 29, 1993.
- 8. FAA. Order 7110.65N, Air Traffic Control. Feb. 21, 2002.
- 9. Ibid.
- International Civil Aviation Organization (ICAO). *Procedures for Air Navigation Services — Rules of the Air and Air Traffic Services.* 13th Edition, 1996. Amendment 3.
 - Seventy events (42 percent) occurred at airports that serve both air carrier aircraft and general aviation aircraft;
 - Military aircraft generated wake turbulence in 10 events (6 percent), nine of which occurred at airports that served both military aircraft and civil aircraft; and,
 - Thirty-four events (21 percent) occurred at airports that serve primarily general aviation aircraft.



Figure 6





Accidents, Incidents Most Often Involved Small Aircraft

Small aircraft were involved more often than aircraft of other weight categories as trailing aircraft in accidents caused by wake turbulence. Of the 130 accidents in the NTSB database, small aircraft were the trailing aircraft in 92 accidents (71 percent); in those accidents, the wake turbulence most frequently (in 29 accidents, or 32 percent) was generated by other small aircraft (Table 5).

Of the 60 incidents in the FAA database, small aircraft were the trailing aircraft in 37 incidents (62 percent; Table 6); of the 37 incidents, 21 incident reports (57 percent) did not specify the type of aircraft that generated the wake turbulence. The reports that included that information said that the wake





turbulence most frequently (in four incidents, or 11 percent) was generated by other small aircraft.

Of the 165 events in the ASRS database, 42 events (25 percent) involved small aircraft as the trailing aircraft (Table 7, page 25). In the 42 events, the wake turbulence most frequently was generated by medium transport aircraft (in 10 events, or 24 percent). (ASRS defines medium transport aircraft as those weighing 30,001 pounds/13,600 kilograms to 60,000 pounds/ 27,200 kilograms.) Four events (10 percent) involved small aircraft that were flown into wake turbulence generated by other small aircraft.

Small Transport Aircraft Involved in Wake-turbulence Accidents

Of the 130 accidents in the NTSB database, 21 accidents (16 percent) involved small transport aircraft (5,001 pounds/2,300 kilograms to 14,500 pounds/6,600 kilograms) as the trailing aircraft (Table 5). Of these, seven accidents (33 percent), including one fatal accident, involved wake turbulence generated by heavy transport aircraft (more than 300,000 pounds/136,000 kilograms).

Of the 60 incidents in the FAA database, nine incidents (15 percent) involved small transport aircraft as the trailing aircraft (Table 6). Of these, four incidents (44 percent) involved aircraft being flown behind medium-large transport aircraft (60,001 pounds/27,200 kilograms to 150,000 pounds/ 68,000 kilograms). The same number of incidents involved wake turbulence generated by aircraft of unspecified size.

Of 165 events in the ASRS database, 15 events (9 percent) involved small transport aircraft as the trailing aircraft (Table 7). Of these, six events involved wake turbulence generated by large transport aircraft (150,001 pounds/68,000 kilograms to 300,000 pounds).

Light transport aircraft were the trailing aircraft in four accidents (3 percent) of the 130 accidents (Table 5). Of the four accidents, two accidents, both fatal, occurred while the aircraft were being flown behind large transport aircraft. Light transport aircraft were the trailing aircraft in five incidents (8 percent) of the 60 incidents (Table 6). Of the five incidents, three incidents involved wake turbulence generated by unspecified aircraft. The other incidents involved wake turbulence generated by one medium-large transport aircraft and one heavy transport aircraft. Light transport aircraft were the trailing aircraft unter 17 ASRS events (10 percent; Table 7). Of the 17 events, eight events (47 percent) involved wake turbulence generated by large transport aircraft.

Pilots of Larger Aircraft Describe Effects of Wake Turbulence During Approach

Of the 130 accidents, medium transport aircraft were the trailing aircraft in six accidents (5 percent; Table 5); of the six accidents, three accidents occurred while the aircraft were being flown behind heavy transport aircraft. Of the 60 incidents, medium transport aircraft were the trailing aircraft in four incidents (7 percent; Table 6); of the four incidents, two incidents occurred while the aircraft were being flown

behind large transport aircraft. Of the 165 events, medium transport aircraft were the trailing aircraft in 28 events (17 percent; Table 7); of the 28 events, 14 events (50 percent) involved wake turbulence generated by heavy transport aircraft.

Medium-large transport aircraft were the trailing aircraft in six of the 130 accidents (5 percent; Table 5). Of these, three accidents involved wake turbulence generated by heavy transport aircraft. Medium-large transport aircraft were the trailing aircraft in four incidents of the 60 incidents (Table 6). Of these, two incidents occurred while the aircraft were being flown behind heavy transport aircraft, and two incidents occurred while trailing aircraft of unspecified weight categories. Medium-large transport aircraft were the trailing aircraft in 27 events (16 percent; Table 7) of 165 events. Of these, 13 events (48 percent) involved wake turbulence generated by heavy transport aircraft.

The following ASRS report was filed by the captain of a McDonnell Douglas MD-82:

Glideslope was out of service. [On final approach] ... at eight [nautical] miles [15 kilometers], I visually acquired my interval aircraft, which was three [nautical miles; 5.6 kilometers] to four [nautical] miles [7.4 kilometers] ahead ... in a steep, descending, left-hand turn to final, 500 [feet] to 1,000 feet above my altitude. ... When it stabilized on final approach course, lacking glideslope guidance, I observed it another [McDonnell Douglas] DC-9-82 type, [which appeared] to be flying a significantly steeper approach than I was. Weather was clear - visibility 10 nautical miles in haze, calm winds at all altitudes below 10,000 feet. Aircraft ahead stabilized 2.5 [nautical miles; 4.6 kilometers] to three nautical miles ahead of my aircraft, [0.5 degree] to one degree above my approach course.

At outer-marker crossing, we switched to ... tower [frequency]. Almost immediately, the aircraft which had been stable and trimmed up at 170 knots, flaps 15 degrees, gear up — rolled approximately 30 degrees to the right, then "snapped" to the left. I applied progressively larger right aileron [input] and right rudder input; however, these seemed to have no effect upon the aircraft's roll rate. The aircraft stopped its roll approximately 70 [degrees] to 80 degrees left wing down, then gradually righted itself, becoming again responsive to the flight controls. The nose lost perhaps five [degrees] to 10 degrees of pitch, but we lost little additional altitude.

I simultaneously added power to correct for the descent and [to] fly a high approach path, completed the "dirty up" [extension of the landing gear and flaps in preparation for landing] on schedule, and made a brief ... announcement to the 80 passengers about

the cause of the roll and [telling them] to not be concerned excessively.

Contributing factors: calm winds, lack of glideslope information, previous aircraft's steep approach, close separation typical of [the airport's] arrival complex, lack of my crew's appreciation for the amount of wake vortex a similar DC-9 aircraft can produce and its effect on other turbojet aircraft.²⁶

An ASRS follow-up interview with the pilot who filed the report revealed the following:

An encounter could have been anticipated, as there were calm winds; no knowledge of the glide [path flown by] the preceding aircraft; [the] preceding aircraft['s] steep approach meant [that the reporting pilot's airplane] would go through the wake somewhere; [the] 2.5-[nautical]-mile separation; and [the] realization that any jet can cause severe turbulence. His ideas for what to do next time are: Fly above [the] other aircraft's glide path, carry an extra 10 knots of speed, be ready for a go-around at any sign of wake turbulence. This [pilot] had no roll control as the encounter progressed. He applied 45 degrees of aileron and heavy rudder, but response to control inputs was slow to take effect. He was positive the bank angle reached at least 70 degrees, if not more, and the event lasted at least six seconds.²⁷

There were no accidents among the 130 accidents in the NTSB database in which large transport aircraft were affected by wake turbulence (Table 5). One of the 60 incidents in the FAA database involved a large transport aircraft being flown behind a heavy transport aircraft (Table 6). Pilots of large transport aircraft filed reports on 25 events (15 percent; Table 7) of the 165 events in the ASRS database. Sixteen of those events (64 percent) occurred while the aircraft were being flown behind heavy transport aircraft.

Educational material typically cautions pilots to avoid wake turbulence generated by heavier aircraft but seldom discusses the possibility of upsets from the wake turbulence of smaller aircraft. Nevertheless, of the 165 events in the ASRS database, nine events (5 percent) involved large transport aircraft following other large transport aircraft, and six of the nine events involved leading aircraft that were smaller than the trailing aircraft.

Pilots of heavy transport aircraft have reported upsets caused by the wake turbulence of lighter aircraft. The 165 events in the ASRS database include four events (2 percent) in which crews of heavy transport aircraft described wake-turbulence upsets — two events involving a medium-large transport aircraft as the leading aircraft and two events involving a large transport aircraft as the leading aircraft (Table 7).

Data Show That 13 U.S. Accidents From 1983–2000 Involved Helicopter Wake Turbulence

Of 130 wake-turbulence accidents in the U.S. National Transportation Safety Board database from 1983 through 2000, 13 accidents (10 percent) occurred when an airplane was flown through wake turbulence generated by a leading helicopter. Four (31 percent) of the 13 accidents occurred when small general aviation aircraft were landing or taking off while helicopters were being hovered near the runway. All 13 accidents occurred within the immediate vicinity of an airport, either on a runway or in a traffic pattern.

Three (5 percent) of 60 wake-turbulence incidents in the U.S. Federal Aviation Administration (FAA) database from 1983 through 2000 involved wake turbulence generated by helicopters.

Of 165 wake-turbulence events reported from 1988 through 1999 to the U.S. National Aeronautics and Space Administration (NASA) Aviation Safety Reporting System (ASRS),¹ 11 events (7 percent) involved airplanes that were flown into wake turbulence generated by military helicopters during night training operations. In six events, the helicopters were being operated with their navigation lights off while the crews used night-vision goggles. In five events, the helicopter crews were communicating on different radio frequencies and were not providing position reports on the common traffic advisory frequency. The airplane pilots were unaware that unlighted helicopters were being flown in the area.

Helicopter wake turbulence results when high-pressure air below the surface of the rotor blades flows around the rotorblade tips into the low-pressure air above the rotor blades.

The wake turbulence takes different forms, depending on how a helicopter is being flown:

- During stationary hovering or a slow hover taxi, a helicopter generates downwash — high-velocity outwash vortices that extend to a distance about three times the diameter of the rotor (Figure 1). The outwash vortices resemble airplane vortices, although the helicopter outwash vortices circulate outward, upward, around and away from the main rotor (or main rotors) in all directions.² FAA says that pilots should not operate small aircraft within three rotor diameters of a helicopter in a stationary hover or a slow-hover taxi;³ and,
- During forward flight, a helicopter generates a pair of spiraling wake vortices from the rotor blades (Figure 2). Wake turbulence also occurs in the rotating air beneath the helicopter.^{4,5} The FAA *Aeronautical Information Manual (AIM)* says that the wake vortices are similar to those of larger fixed-wing aircraft. FAA says that pilots of small aircraft should use caution when trailing helicopters in forward flight.⁶

A 1962 report on flight tests by the NASA Langley Research Center to examine the in-flight characteristics of helicopter



Figure 2

wake turbulence said that roll rates of more than 36 degrees per second resulted when a two-place, tricycle-gear military training airplane was flown into the wake turbulence of a three-blade, single-rotor helicopter 100 feet below and 200 feet below the helicopter's flight path. The airplane's induced bank angles were 40 degrees. Flight into wake turbulence during a descent resulted in moderate rolling and a doubled descent rate. The test helicopter weighed 6,900 pounds (3,130 kilograms) and had a rotor diameter of 53 feet (16 meters); the test airplane weighed 7,400 pounds (3,357 kilograms) and had a wingspan of 41 feet (13 meters).⁷

Another flight-test program was conducted in 1991 by FAA. Helicopters of various sizes were used: a Bell UH-1H, a Sikorsky S-76A, a Sikorsky UH-60 Black Hawk, a Sikorsky CH-53E Super Stallion and a Boeing Vertol CH-47D Chinook. Each helicopter was outfitted with a smoke-generating device to mark the helicopter's wake turbulence.⁸

The test airplanes were a Beechcraft T-34C — a 4,300-pound (1,950-kilogram), 715-horsepower (533-kilowatt [kW]),

low-wing turboprop monoplane with a 33-foot (10-meter) wingspan — and a Bellanca 8KCAB Super Decathlon — an 1,800-pound (816-kilogram), 180-horsepower (134-kW) highwing reciprocating-engine airplane.

FAA found similarities in the wake turbulence of airplanes and helicopters. In both categories of aircraft, wake vortices generated at low airspeeds initially were more intense than those generated at higher airspeeds, heavier aircraft generated more intense wake vortices than lighter aircraft, and larger aircraft generated larger wake vortices than smaller aircraft.

The wake vortices generated by a helicopter's advancing blade and by its retreating blade are different. Because the retreating blade operates at a lower relative airspeed, it must have a higher angle-of-attack to produce as much lift as the advancing blade. As a result, the wake vortices behind the advancing rotor blade are consistently smaller and more coherent, especially as the helicopter's forward speed increases above 80 knots. The wake vortices behind the advancing rotor blade result in more abrupt roll excursions and yaw excursions in the trailing aircraft than the retreatingblade vortices. In the flight tests, the vortices behind the retreating blade were characterized by a larger diameter, less-dense smoke marking and a greater cross-sectional area.

The wake vortices were was generated differently, depending on whether the helicopter was ascending or descending. The vortex cores were observed moving farther apart during descents and closer together during ascents.

The helicopter wake vortices did not sink in a predictable manner, perhaps because a large amount of power was required to generate lift and, as a result, hot exhaust was trapped in the wake vortices. The hot exhaust contributed to the buoyancy of the wake vortices.

The area affected by the wake turbulence of a helicopter is larger than the area affected by the wake turbulence of an airplane of comparable size and weight, especially at speeds below 70 knots to 80 knots. The number of rotor blades appears to affect the size of a helicopter's wake vortex. For example, the UH-1H — with two blades — generated smaller wake vortices than the S-76A — with four blades — even though both helicopters are about the same weight. (The UH-1H has a maximum certificated takeoff weight [MCTOW] of 9,500 pounds [4,309 kilograms], and the S-76A has a MCTOW of 10,000 pounds [4,536 kilograms]. Both have main rotors with 44-foot [13-meter] diameters.)

In the 1991 FAA flight tests, the airplane pilots conducted "parallel" entries and "cross-track" entries into the helicopter's wake turbulence. A parallel entry occurs when a trailing aircraft is flown behind and below the leading aircraft (the aircraft generating wake turbulence) in about the same direction. This can cause an intense rolling reaction when an aircraft is flown into the wake turbulence. A cross-track

entry involves an aircraft flown through wake turbulence at a large angle. Cross-track entries usually result in short, sharp vertical jolts with little roll or yaw; in these occurrences, the primary risk is to the structural integrity of the aircraft.⁹

FAA test pilots flew the airplanes into the helicopters' wake turbulence in parallel entries by flying above, below, left and right of the vortices. At small separation distances, the airplanes typically experienced more severe upsets (in the form of roll, pitch and/or yaw excursions) when the helicopters were flown at slower speeds. Smaller separation distances, resulted in loss of control; at larger separation distances, upsets typically were more severe.

In the flight tests, the airplanes had the following reactions:

- The T-34C recorded induced bank angles of 45 degrees when being flown about one nautical mile (1.9 kilometers) behind the Black Hawk, which has a maximum takeoff weight of 20,250 pounds (9,185 kilograms) and four rotor blades with a rotor diameter of about 53 feet (16 meters). The Black Hawk was being flown at 70 knots to 80 knots. When the separation distance was reduced to 0.5 nautical mile (0.9 kilometer), induced bank angles increased to 75 degrees to 90 degrees. When the helicopter was flown at a slower speed (thus generating more intense vortices), the T-34C was rolled beyond 90 degrees when it was flown one nautical mile behind the Black Hawk and rolled beyond 180 degrees when flown 0.5 nautical mile behind the Black Hawk;
- The T-34C was rolled between 30 degrees and 75 degrees while flying between three nautical miles (5.6 kilometers) and five nautical miles (9.3 kilometers) behind the UH-1H; several of the test points caused much more pronounced roll excursions and led to loss of control and spins;
- The Chinook, a heavy-lift helicopter with a tandemrotor configuration, an MCTOW of 50,000 pounds (22,680 kilograms) and a 60-foot (18-meter) rotor diameter, generated wake turbulence strong enough while being flown at 120 knots to roll the test airplanes 90 degrees. At distances less than 0.8 nautical mile (1.5 kilometers), the roll excursions varied from 90 degrees to 210 degrees, and many roll excursions resulted in loss of control and spins;
- The Super Stallion, with an MCTOW of 69,750 pounds (31,639 kilograms) and a seven-blade rotor system with a 79-foot (24-meter) diameter, generated wake vortices that rolled the trailing aircraft more than 90 degrees with a separation distance of one nautical mile. At 0.5 mile, the trailing aircraft rolled nearly 180 degrees and entered a spin; and,
- Several flight tests with the Super Decathlon behind the CH-53E were halted when the Decathlon

unexpectedly shuddered, which the test pilot characterized as a "flapping of the wings." The tests were stopped because of the risk of catastrophic wing flutter. The engineers said that the vortices of the individual rotor blades were present in the overall wake-turbulence pattern downstream from the helicopter and that the individual vortices probably created the rhythmic pattern.◆

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- 3. FAA. *Aeronautical Information Manual (AIM)*. Chapter 7, Section 3: Wake Turbulence.
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The following ASRS report was filed by the pilot of a B-757 (categorized by ASRS as a large transport aircraft):

I was flying a B-757 on an approach to Runway 22L. The wind at the time was reported [from 190 degrees at 10 knots]. We had been following a B-727 by only approximately 2.5 [nautical] miles. ... This did not seem to be a problem, as we did not feel any unusual turbulence during the approach. The B-727 landed and turned off the runway.

At approximately 50 feet AGL (on speed and glideslope), the aircraft suddenly began a hard, rapid roll to the left. I tried to counteract with right-aileron input, but it took almost full right aileron to stop the roll. ... After a slight hesitation, the aircraft began to respond and roll back toward the right. I started to release the right-aileron input. ... However, as soon as the right-aileron pressure was eased, another rapid

left roll began. I ... reached full right-aileron input just prior to left wheels ground contact. As the left wheels hit the ground, a rapid roll to the right began, and the left wing attempted to lift from the ground. I pushed the nose forward in an attempt to get, and keep, both wheel trucks on the ground. This action worked and the nosewheel was lowered normally.

Rollout was uneventful. I can think of no phenomena that could have caused this event except possibly the vortices from the B-727 that landed just ahead of us.²⁸

An ASRS follow-up interview with the pilot who filed the report revealed the following:

The first officer said that the weather conditions were good, occasional light turbulence with the winds [from] 180 degrees at eight knots. He [said that he] was flying the B-757-200 at "bug [landing reference speed] plus five knots, and everything was perfect until the roll started." The B-727 ahead of [his] aircraft did not report any disturbances. At about 50 feet, the initial roll began. Then, just prior to touchdown, the second roll started. ... [He said that] the first roll took "all of the aileron authority I had, and when the second one began, I decided that I had better put the aircraft on the runway." The touchdown was firm. The first officer, who had been a highly experienced captain at another air carrier, stated that he had not experienced such persistent roll in a wake before this.²⁹

Wake Turbulence Cited in One Heavy Transport Aircraft Accident

The NTSB database includes one accident in which a heavy transport aircraft was affected by wake turbulence (Table 5). The leading aircraft also was a heavy transport aircraft. There were no incidents in which heavy transport aircraft were the trailing aircraft. The ASRS database includes 11 events (7 percent) in which heavy transport aircraft were flown into wake turbulence (Table 7). In seven of those events (64 percent), the wake turbulence was generated by another heavy transport aircraft.

The following ASRS report was filed by the captain of a McDonnell Douglas DC-10:

We intercepted final about five [nautical] miles [9.3 kilometers] outside the final approach fix and proceeded to fly a normal approach using the FMS/ ILS [flight management system/instrument landing system] and standard air carrier procedures. An approach check was re-accomplished to identify the Runway 36R localizer and confirm the new minimums for that approach. The first officer flew the FCP [flight control panel] until we broke out of the weather after crossing the final approach fix. We checked in with [the] tower and were cleared to land on Runway 36R. At about 500 feet AGL, the copilot disconnected the autopilot and began to hand-fly the aircraft, with the autothrottles still connected. Since the aircraft had been fully configured for landing earlier, the autopilot had it trimmed up, and I did not detect major trim changes ... by the copilot, nor did the "stabilizer motion" alert sound after the autopilot was disconnected. The approach was flown on course and glide path. Later analysis of the flight data recorder did not show any discernible difference between the autopilot and the copilot flying. A wellstabilized, power-on approach was flown down to about 100 feet AGL.

As the runway threshold lights were passing under the nose, the aircraft entered into a series of abrupt and violent roll excursions, which I estimate to be in the range of 15 [degrees] to 20 degrees of bank. There were three or four of these roll reversals, which ended as abruptly as they began. At this point, I would estimate the aircraft altitude at about 15 feet, with the nose slightly higher than the normal flare attitude. The aircraft seemed to hang there for a second, and then the nose came down, and we touched down very hard in what felt like a flat, three-point touchdown. The nose rose up in the air and then settled back to the runway. I took control of the aircraft immediately after touchdown because I anticipated blown tires or steering problems, but there were none. I slowed the aircraft and taxied to the ramp.

The entire episode — violent rolls, ending of the roll motions prior to landing and then the hard landing - lasted about three [seconds] to four seconds. It seemed to me that all this started at about the point where a flare would be initiated. Given the short, abrupt and violent nature of these gyrations, I didn't have a chance to call for a go-around, much less assume control and accomplish [a go-around]. Later analysis of the flight data recorder confirms my recollection of this incident. The data trace shows abrupt and rapid roll excursions, which end as suddenly as they begin, followed by a second or so of level flight and then a g-load spike [sudden increase in gravity-loading], which occurs on the hard touchdown. Given the stabilized approach flown by the first officer, I would discount the probability of pilot-induced oscillations, at least with the beginning of the roll excursions. Furthermore, the sudden onset and termination of the roll motions tell me that the roll inputs of the first officer were in reaction to external forces and [the first officer] succeeded in damping them out prior to touchdown.

The tower winds at the time were northwesterly at seven knots, less than reported on ATIS [automatic terminal information service]. We landed one minute behind a large transport, and our landing gross weight was 429,000 pounds [194,595 kilograms], well below the maximum of 471,000 [pounds (213,646 kilograms)] for the wide-body. I would speculate that the upwind ... vortex from the large transport would drift over the runway threshold in that amount of time, which would cause at least the initial roll motion at precisely the time when our aircraft was most vulnerable.³⁰

A follow-up interview by ASRS with the pilot who filed the report revealed the following:

The closest preceding aircraft was a large transport [that had] landed three minutes 50 seconds earlier. No known

Atmospheric Conditions, Aircraft Characteristics Determine Intensity of Wake Vortices

The initial intensity of wake vortices is determined primarily by the weight, speed, configuration, wingspan and angle-ofattack of the leading aircraft (the aircraft generating the wake vortices). The most important variables in determining the intensity of a vortex beyond a distance of 10 wingspans to 15 wingspans from the leading aircraft are atmospheric stability, wind, ground effect and turbulence.¹

Development of a wake vortex occurs in several stages.^{2,3}

The first stage is formation of the vortex. Current aerodynamic theory models the airflow over the wing as a series of wake vortices. A dominant pair of vortices absorbs the weaker vortices, rolling into a "trailing edge vortex sheet," which then rolls into a more coherent, or more unified, vortex. This roll-up occurs within two wingspans to four wingspans behind the aircraft.⁴

Space Administration (NASA), vortices created by a heavy transport aircraft (maximum gross weight of 300,000 pounds/ 136,000 kilograms, wingspan of 140 feet [43 meters] and approach speed of 150 knots) sank at 350 feet per minute (fpm). Vortices generated by an aircraft with a maximum gross weight of 35,000 pounds (15,876 kilograms), wingspan of 95 feet (29 meters) and approach speed of 100 knots settled at 150 fpm.⁶

Research on Boeing 727, 757 and 767 airplanes found that the rate at which wake vortices sink depends on aircraft configuration, atmospheric conditions and aircraft/vortex proximity to the ground. Table 1 shows the sinking rates of vortices and the approximate altitudes where ground effect becomes a factor. In general, vortices that form from wings with extended flaps sink more rapidly than vortices that form from wings with retracted flaps.⁷

Table 1Characteristics of Vortex Motion by Aircraft Type and Configuration

| Airplane Model | | Separation of Vortex Pair (aircraft gear and flaps retracted) | Separation of Vortex Pair (aircraft in landing configuration) | Height of Ground Effect (aircraft gear and flaps retracted) | Height of Ground Effect (aircraft in landing configuration) | Vortex Sink Velocity (aircraft gear and flaps retracted) | Vortex Sink Velocity (aircraft in landing configuration) |
|-------------------------|---------------------------|--|--|--|--|---|---|
| Boeing 727-100/ -222 | 108.0 feet 32.9 meters | 85.0 feet 26.0 meters | 65.0 feet 20.0 meters | 42 feet AGL | 33 feet AGL | 8.2 fps 2.5 mps | 10.7 fps 3.3 mps |
| Boeing 757-200 | 124.8 feet 38.1 meters | 98.0 feet 30.0 meters | 74.0 feet 23.0 meters | 49 feet AGL | 37 feet AGL | 7.4 fps 2.3 mps | 9.9 fps 3.0 mps |
| Boeing 767-200 | 156.0 feet 47.6 meters | 123.0 feet 38.0 meters | 82.0 feet 25.0 meters | 61 feet AGL | 41 feet AGL | 6.2 fps 1.9 mps | 9.3 fps 2.8 mps |

AGL = Above ground level fps = Feet per second mps = Meters per second

Source: Patrick R. Veillette, Ph.D., from data in "Vortex Characteristics of B-757-200 and 767-200 Aircraft Using the Tower Fly-by Technique," by Leo J. Garodz and Kirk L. Clawson. U.S. National Oceanic and Atmospheric Administration Technical Memorandum ERL ARL-199. Air Resources Laboratory, Silver Spring, Maryland, U.S. January 1993.

The second phase of wake-vortex development involves the effects of the vortices on each other. Each vortex induces an airflow pattern (called a velocity field) that causes the other vortex to sink. Additionally, because of the generation of lift on the wing, there is an equal and opposite reaction on the airflow, which induces a downward motion.

If no other factors influenced vortex motion, the two vortices would sink in this stable manner, remaining a constant distance from each other, until they are 100 feet to 200 feet above ground level (AGL). Then they would slow and move outward, away from each other, at a speed of two knots to three knots.⁵

The actual sinking velocities of the wake vortices may vary. In flight tests by the U.S. Air Force, the U.S. Federal Aviation Administration (FAA) and the U.S. National Aeronautics and (Although all airplanes generate wake vortices, most of the studies cited in this report examined the wake-vortexgenerating characteristics of Boeing airplanes — which comprised the largest percentage of the U.S. fleet during the 1970s, 1980s and 1990s, when the studies were conducted.)

Peak velocities within the vortex core (tangential velocities) can attain high values. For example, a peak velocity of 326 feet (99 meters) per second was recorded during research involving a B-757 in the landing configuration being flown on a three-degree glideslope.⁸

The third phase of wake-vortex development is distinguished by the growth of the vortex axis and possible wavelength disturbances (in which the vortex develops waves). Several

critical parameters, such as atmospheric turbulence, can increase wavelength disturbances that eventually result in dissipation of the vortex.⁹ Because the vortex remains highly coherent during this phase, the hazard to aircraft persists.

During the fourth phase, wavelength disturbances can increase. Often, the two vortices link together at points of minimum separation (the locations where waves in the two vortices are close together), and the linkages lead to a series of vortex rings (in which the airflow no longer rotates around a horizontal axis but moves instead around a circle) and a further decrease in vortex intensity.¹⁰ Linking is the primary means by which vortices lose intensity in air that is free of atmospheric turbulence.^{11,12,13} In atmospheric turbulence, wake vortices lose intensity through vortex "bursting" — a condition in which the structure of a vortex changes abruptly. Bursting is the most common form of vortex dissipation in turbulent atmospheric conditions.¹⁴

The fourth phase also involves the sudden increase in the size of the core of the vortex, followed by a decrease in tangential velocity. Often during this phase, the vortices change orientation and become distorted, resulting in turbulent airflow.¹⁵

Sometimes, wake vortices can be heard. Researchers who have been beneath the final-approach paths of landing jet aircraft — especially B-757-200 and B-767-200 aircraft — have heard a whistling sound that they have attributed to the shearing action between the tightly rolled vortices and the surrounding air mass. Researchers have described the sound as similar to that generated by an artillery shell passing overhead. Whistling sounds also have been heard from B-727-100 aircraft.^{16,17}

In flight tests, the intensity of the vortex whistling sound varied, depending on flap configuration. The B-767-200 whistling sound became louder as flaps were retracted and became a "roar" when the flaps were fully retracted for two holding-configuration tests. The most repeatable whistling sound occurred when the B-767 was in takeoff configuration with the flaps set at one degree (in that configuration, leading-edge devices on the B-767 also are deployed).¹⁸

Temperature Gradient Remains Primary Predictor of Wake-vortex Intensity

The most reliable predictor for wake-vortex intensity and persistence is the atmospheric temperature gradient.¹⁹ As vortices sink, they are affected by viscous forces (in which the viscosity of the atmosphere extracts energy from the vortices and reduces their strength) and buoyancy forces (in which vortices move upward because they are less dense than the surrounding atmosphere).

As a wake vortex sinks, it is compressed by increasing atmospheric pressure, and the temperature within the wake vortex increases. The warming of a wake vortex adds to its buoyancy, which in some temperature conditions can cause the wake vortex to maintain a constant height, rather than to continue sinking; sinking would be more characteristic behavior.²⁰

Testing at the Idaho (U.S.) Nuclear Engineering Laboratory (INEL) found that the most persistent wake vortices and the most intense wake vortices were generated in a "neutrally stable" atmosphere.²¹ A neutrally stable atmosphere is a condition in which the atmospheric temperature changes at a rate equivalent to the rate of temperature change within the wake vortex. The resulting neutral buoyancy causes the vortices to remain at a relatively constant altitude. In other tests of wake vortex activity in a neutrally stable atmosphere, wake vortices persisted longer than 3.5 minutes and were moved more than 1,640.5 feet (500 meters) downwind by winds of about six knots to 10 knots.²²

The phenomenon of the neutrally stable atmosphere helps to explain why some trailing aircraft are flown into wake vortices long after the leading aircraft has passed. Atmospheric conditions that are less stable than the neutrally stable atmosphere result in faster dissipation of wake vortices.

The general relationship between atmospheric turbulence and vortex intensity was discovered during flight tests at INEL that showed that nearly all vortices with tangential velocities of more than 142 knots (or 240 feet [73 meters] per second) developed in conditions of a near neutrally stable atmosphere. The recorded data showed that many of the vortices persisted at fairly high tangential velocities for more than 60 seconds, even with relatively unstable conditions in the atmosphere.

The effects of turbulence on vortex persistence have been the subject of several studies.^{23,24,25,26} Nevertheless, many details of the relationship between turbulence and vortex persistence are not well understood,²⁷ and direct measurement of atmospheric turbulence is difficult.

Near the Ground, Vortices Decelerate and Separate

The behavior of wake vortices at very low altitudes differs from wake-vortex behavior at higher altitudes and has been the subject of many scientific studies.

Research conducted during the 1990s found that vortices generated when the aircraft is being flown in ground effect typically do not sink — and that suggests that pilots of trailing aircraft may not have sufficient time or sufficient altitude to recover their aircraft from the influence of the vortex-induced motion.²⁸ A 1982 report by the U.S. Department of Transportation had said that wake vortices separate and rebound (move higher into the air) after reaching the ground.²⁹

The ground modifies the trajectory of a wake vortex generated during takeoff and landing by acting as a reflection

plane so that the vortex — after striking the ground — rebounds.³⁰ In a 1991 study, vortices generated near the ground by a B-767 were observed to move above the point where they were generated.³¹ Researchers also have said that wake vortices can "bounce" from the ground to heights equal to twice the wingspan of the vortex-generating aircraft.^{32,33} The FAA *Aeronautical Information Manual (AIM)*, however, says that "no one can say what conditions cause vortex bouncing, how high they bounce, at what angle they bounce, or how many times a vortex may bounce."³⁴

As a vortex sinks close to the ground, it creates a secondary vortex rotating in a direction opposite that of the primary vortex. One of the effects of the secondary vortex is to induce upward movement of the primary vortex.³⁵ Studies show that such an upward movement is more pronounced when the surrounding air is smooth than when the surrounding air is turbulent.³⁶ Thus, some vortices may be present in locations where pilots may not anticipate them. For example, pilots who fly their aircraft on a higher glide path as a preventive measure inadvertently may position their aircraft near wake vortices.

Winds, Atmospheric Turbulence Influence Wake-vortex Development

Research has shown a correlation between wind, the movement of the vortex and the persistence of the vortex. The most persistent vortices during crosswind conditions are upwind vortices, which linger at the approach end of the active runway and typically gain intensity because of the influence of the crosswind.³⁷ Because the ambient wind speed (the wind speed in the air surrounding a vortex) is greater at the top of the vortex than at the bottom, the crosswind increases the upwind vortex rotation.³⁸ In contrast, the crosswind diminishes the intensity of the downwind vortex.

Ambient wind speed also is associated with vortex persistence. In flight tests involving military transport aircraft (Lockheed C-130E, Lockheed C-141B and Lockheed C-5A/B), wake vortices were persistent when winds were from three knots to 10 knots.³⁹ Vortices that persisted longer than 60 seconds generally were generated during winds of three knots to 10 knots; stronger winds dissipated vortices more quickly.

During tests involving B-727, B-757 and B-767 aircraft, all vortices that persisted longer than 85 seconds were generated when the wind speed was less than five knots. Vortices that persisted longer than 35 seconds were generated when the wind speed was 10 knots or less. All vortices with tangential velocities of more than 200 feet per second were generated when ambient wind speeds were from five knots to 10 knots. Higher ambient wind speeds and stronger wind shear typically led to dissipation of vortices. Nevertheless, low wind speeds indicated less atmospheric turbulence and were associated with more persistent vortices. The most persistent vortices were generated during ambient wind speeds from three knots to five knots.⁴⁰

Slower Aircraft, Smaller Wingspans Generate More Intense Vortices

Aircraft speed and size also influence wake-vortex generation and dissipation, and the severity of a wake-turbulence occurrence. For example, more intense vortices are generated as an aircraft slows because there is greater circulation of air around the wing. (The lift of a wing is proportional to the circulation of air around it. Greater circulation of air creates greater lift. At a constant angle-ofattack, higher airspeed creates greater lift. As an aircraft slows, less air moves over the wing, and to create the same amount of lift, the aircraft must be flown at a higher angleof-attack. As the angle-of-attack is increased, the circulation increases.) Aircraft with smaller wingspans generate more intense wake vortices than aircraft with equivalent weights and longer wingspans; this is because the vortex is generated within a smaller distance. Heavier aircraft generate more intense vortices because of their greater lift requirements.

Studies of the effect of wake vortices generated by aircraft with large wingspans have found that vortices can cause a reduction of lift on a trailing aircraft. This effect becomes more significant as the angle-of-attack of the leading aircraft is increased. For example, if the leading aircraft is flown at an angle-of-attack of about eight degrees, the wing of the trailing aircraft experiences a zero-lift angle-of-attack of nearly seven degrees and a 30 percent decrease in the maximum lift coefficient.⁴¹

Airplanes with flaps extended produce multiple vortices, which weaken somewhat as they merge. The extra drag and turbulence produced by flap extension accelerate dissipation. On most airplanes, the greater the flap extension, the weaker the tangential speed of the wake vortices.

There are exceptions, however. The B-757 wing was designed so that, when flaps are extended, lift is distributed more evenly across the entire wing, compared with other wings. When the flaps are extended, the B-757 has a continuous wing-flap trailing edge with no cutouts (gaps) between the inboard flaps and outboard flaps in the jet-exhaust area. The result is relatively even wingspan load distribution. The absence of cutouts decreases or eliminates the generation of multiple vortices when the airplane is in the landing configuration at various settings of flaps and wing-tip leading-edge devices. Multiple vortices typically interact with each other, causing a decrease in vortex tangential velocities downstream from the airplane. The geometry of the B-757 wing — with a relatively low wing sweep of 25 degrees and a relatively straight trailing edge - also may contribute to the decrease in tangential velocities.42,43 In flight tests with the aircraft in landing configuration on a three-degree glide path, the tangential velocity of the wake vortices created by the B-757 (at 193 knots) was 50 percent higher than the tangential velocity created by other aircraft tested.44

A 1994 report by the U.S. National Transportation Safety Board (NTSB) said that NTSB had studied five waketurbulence accidents and incidents from December 1992 through December 1993 in which B-757s were the leading aircraft. The report said that NTSB initially focused on why the B-757 apparently had been involved in a disproportionate number of wake-vortex occurrences and found "little technical evidence to support the notion that the wake vortex of a B-757 is significantly stronger than indicated by its weight."⁴⁵

The report said that most researchers believe that the primary factor in determining the risk associated with wakevortex occurrences is not the airspeed within the core of the vortex but the vortex circulation, a measure of the angular momentum of the air in the airflow field. The report said that the B-757's vortex circulation was greater than that of the B-727 and less than that of the B-767. Flight tests by the U.S. National Oceanic and Atmospheric Administration, however, produced different results. In those tests, the B-757 showed the highest average vortex circulation — 1,173 feet (358 meters) per second — during flight tests of the three aircraft. The B-757's vortex circulation from the heavier B-767.⁴⁶

Research using the C-130 showed little correlation between vortex speeds and flap deflection. The C-130's four turboprop engines accelerate the air behind the engine nacelles to create a localized high-velocity airflow pattern in four areas along the wing. This high-velocity flow-field creates turbulence, which has a twofold effect. First, the turbulence breaks up the coherence of the overall wake vortex and reduces its intensity. Second, turbulence accelerates the dissipation of a vortex. As the flaps are extended, additional engine thrust is required, creating additional turbulence within the developing vortex. Light transport aircraft with similar engine configurations may have similar wake-vortex generating characteristics.⁴⁷

Flap design also affects the behavior of wake vortices. Studies of various Airbus aircraft found that the A320 and the A321 have different wake-vortex patterns, apparently because the A320 has single-slotted flaps and the A321 has double-slotted flaps.⁴⁶ (Other studies of the A321 found that vortices that formed around the flaps were more intense than vortices that formed around the wing tips. Similar studies of an A310, however, showed that flap vortices and wing tip vortices were the same intensity.)⁴⁹

Low-slung engines, such as those on the C-141 and C-5A, diminish the interaction of wake vortices with jet engine exhaust, thus increasing vortex persistence. Engines that are low enough below the wing that no flap cutouts are needed preclude the generation of multiple-flap vortices, which typically would accelerate vortex dissipation during takeoff or landing.⁵⁰

The engine exhaust plume may affect vortex motion in another way. The extent to which exhaust gas is trapped in the air in sinking vortices depends on the location of the engines and the location of the wake-vortex cores. Studies of the trapped portions of exhaust plumes have found that these portions of exhaust plumes are cooled in a different way than the portions of exhaust plumes that are not trapped within the vortex. Because of the intense confining effect of the vortex core, the temperature of the vortex core affects vortex motion.⁵¹ Engine exhaust is warm, and on some aircraft in certain configurations, the warm exhaust is trapped in the wake vortices. The warm air resists the settling motion of the vortices and acts as a buoyancy force that keeps the vortices aloft.⁵²

The position of the landing gear also affects wake-vortex generation. An extended landing gear produces an airflow disturbance that helps to dissipate wake vortices.

Other variations in wake-vortex behavior are associated with wing configurations (high-wing or low-wing) and the type of aircraft tail (T-tails or conventional tails). All the military transport aircraft tested (C-5A, C-141B and C-130) have high wings and high aspect ratios. Researchers have said that, because of the induced-drag characteristics and interference-drag characteristics of these aircraft, the undisturbed flow of air over the top of the wing provides more lift than mid-wing designs or low-wing designs.⁵³

The T-tail surface is a lifting surface, although the lift is produced in the downward direction. The high T-tails on the B-727, C-5A and C-141 may contribute to the persistence of vortices. The T-tail produces its own pair of vortices, above and separate from the wing. These T-tail vortices typically are not integrated into the wing vortices or the downwash field. High T-tail designs result in little interaction or no interaction between the wing vortices and the T-tail vortices. Embedded vortices are more likely to be generated by aircraft with conventional tails, such as the B-737 and B-747.⁵⁴

Other factors that determine the severity of a waketurbulence occurrence include the trailing aircraft's design characteristics. A lighter aircraft, for example, is more likely to be upset by wake turbulence than a heavier aircraft. The distribution of weight within the trailing aircraft also is a factor because aircraft with weight concentrated in the wings have more resistance to induced rolling forces.

The wingspan of the trailing aircraft affects the pilot's control of the aircraft's reaction to wake turbulence. If the wingspan of the trailing aircraft is greater than the diameter of the wake vortex from the leading aircraft, ailerons may help counteract the roll. If the wingspan of the trailing aircraft is smaller than the vortex diameter, however, the ailerons will be within the vortex and, therefore, less able to counteract the roll.

In NASA flight tests in 1971, a Lockheed C-5A at 12,000 feet was trailed in different flights by a McDonnell Douglas DC-9, a Cessna 210 and a Gates Learjet. Flight into the C-5A's wake vortices resulted in bank angles of more than 30 degrees for the trailing aircraft at separation distances of about eight nautical miles (15 kilometers) and a time lapse of 2.7 minutes. The wake vortices sank nearly 1,300 feet below the C-5A's altitude about three minutes after aircraft passage, and the vortices remained intact for more than 10 nautical miles (19 kilometers) behind the aircraft — about three minutes after the aircraft's passage. The tangential velocity was measured at about 3,600 feet (1,098 meters) per minute as far as 1.5 nautical miles (2.8 kilometers) behind the C-5A, or for 30 seconds after the aircraft's passage.⁵⁵♦

- Patrick R. Veillette, Ph.D.

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left-main gear first, bounced and then landed flat on all three gear simultaneously." $^{\!\!\!\!\!^{31}}$

A 1991 report on 140 wake-turbulence events reported to ASRS from 1983 through 1990 said that more than half of all reported wake-turbulence occurrences in the United States occurred between transport aircraft. The report said that in 40 percent of the events, the leading aircraft was a heavy aircraft (defined by FAA at the time as weighing more than 300,000 pounds), and in 53 percent of the events, the leading aircraft was a large aircraft (then defined by FAA as weighing more than 12,500 pounds/ 5,670 kilograms to 300,000 pounds). The trailing aircraft was a large aircraft (then defined by FAA as weighing 12,500 pounds or less) in 36 percent of the events. Twenty-five percent of the events involved a large aircraft trailed by another large aircraft, 22 percent

Table 7Weight Categories of Trailing Aircraft and Leading (Wake-generating)Aircraft in U.S. Wake-turbulence Events, 1988–1999

| Leading | | | | | | ng Aircraft | | | | |
|------------|-------------------------------|--------------------|---------------------------------|---------------------------------|----------------------|----------------------------|---------------------------------|---------------------------------|--------------|--|
| | Categories | Small ¹ | Small Transport ² | Light Transport ³ | Medium Transport⁴ | Medium-large Transport⁵ | Large Transport ⁶ | Heavy Transport ⁷ | Row Total | |
| | Small ¹ | 4 | 3 | 7 | 10 | 7 | 5 | 6 | 42 | |
| | Small Transport ² | - | _ | - | 2 | 2 | 6 | 5 | 15 | |
| aft | Light Transport ³ | - | _ | - | 2 | 1 | 8 | 6 | 17 | |
| Aircraft | Medium Transport ⁴ | - | - | - | 2 | 2 | 10 | 14 | 28 | |
| Trailing A | Medium-large Transport⁵ | _ | _ | _ | 2 | 3 | 9 | 13 | 27 | |
| rail | Large Transport ⁶ | - | - | - | - | - | 9 | 16 | 25 | |
| F | Heavy Transport ⁷ | - | - | - | - | 2 | 2 | 7 | 11 | |
| | Column Total | 4 | 3 | 7 | 18 | 17 | 49 | 67 | 165 | |

Note: Numbers in kilograms have been rounded.

¹ U.S. National Aeronautics and Space Administration (NASA) Aviation Safety Reporting System (ASRS) defines small aircraft as weighing 5,000 pounds/2,300 kilograms or less.

² NASA ASRS defines small transport aircraft as weighing 5,001 pounds/2,300 kilograms to 14,500 pounds/6,600 kilograms.

³ NASA ASRS defines light transport aircraft as weighing 14,501 pounds/6,600 kilograms to 30,000 pounds/13,600 kilograms.

⁴ NASA ASRS defines medium transport aircraft as weighing 30,001 pounds/13,600 kilograms to 60,000 pounds/27,200 kilograms.

⁵ NASA ASRS defines medium-large transport aircraft as weighing 60,001 pounds/27,200 kilograms to 150,000 pounds/68,000 kilograms.

⁶ NASA ASRS defines large transport aircraft as weighing 150,001 pounds/68,000 kilograms to 300,000 pounds/136,000 kilograms.

⁷ NASA ASRS defines heavy transport aircraft as weighing more than 300,000 pounds/136,000 kilograms.

Source: Patrick R. Veillette, Ph.D., from U.S. National Aeronautics and Space Administration Aviation Safety Reporting System data on 165 events

involved a large aircraft trailed by a heavy aircraft, and 21 percent involved a large aircraft trailed by a small aircraft.³²

Most Wake-turbulence Accidents Occur In Visual Meteorological Conditions

Most wake-turbulence accidents, incidents and events in the author's study occurred in VMC. Of the 130 accidents in the NTSB database, 127 accidents (98 percent) occurred in VMC. Of the 60 incidents in the FAA database, 59 incidents (98 percent) occurred in VMC. Of the 165 events reported to the ASRS database, 143 events (87 percent) occurred in VMC. Day lighting conditions prevailed during 124 accidents (95 percent), all 60 incidents and 124 events (75 percent). Night lighting conditions prevailed during four accidents (3 percent) and 41 events (25 percent). Lighting conditions were not specified in two accident reports.

Air traffic controllers are required to provide lateral separation guidance and vertical separation guidance between aircraft that are operated under instrument flight rules and that are receiving air traffic control (ATC) services. The separation criteria are intended to minimize the risk of midair collisions and wake-vortex occurrences. Controllers may issue a clearance for a visual approach when an aircraft is the first one in an approach sequence, when an aircraft crew is told to follow a leading aircraft and the crew says that the leading aircraft is in sight, or when a crew says that the airport or the landing runway is in sight but the leading aircraft is not in sight. (In that situation, radar separation must be maintained by ATC until the leading aircraft is in sight and visual separation can be maintained.)

During peak traffic periods, controllers use visual approaches to increase traffic capacity and to reduce delays. Pilots may accept visual-approach clearances, yet be unable to maintain adequate separation from the leading aircraft without additional maneuvering, reconfiguration of the aircraft or reductions of airspeed. Thus, a "compression effect" can be created in which the risk of a wake-turbulence occurrence increases for each successive arriving aircraft.

Thirty-seven of the 165 reports in the ASRS database (22 percent) involved events that required extensive maneuvering to maintain safe separation. Fifteen reports (9 percent) referred to events in which ATC had requested "tight patterns" or had used similar phrases. ATC instructions were cited in 24 reports (15 percent) as contributing factors to wake-vortex occurrences.

The following ASRS report was filed by the captain of a Dassault Falcon 10C:

TRACON [terminal radar approach control] cleared my aircraft for a visual approach to Runway 35R to follow a B-757 turning right base to final — also on a visual approach. Our separation from the B-757 was six [nautical] miles [11 kilometers], as reported by the approach controller. I briefed my copilot regarding my intentions to avoid the vortices of the B-757: We would maintain a glide path at least one dot above the glideslope and fly an airspeed of V_{REF} [landing reference speed] plus 15 knots.

After the briefing, approach control issued instructions for me to maintain an airspeed of 180 knots to the outer marker. I complied with the instructions and observed the B-757 fly what appeared to be a visual approach that was on the glideslope. [The B-757's] touchdown point on the runway was between the 1,000-foot [marker] and 1,500-foot marker [305-meter marker and 458-meter marker]. I continued my approach and maintained a flight path one [dot] to two dots above the glideslope. At approximately 350 feet AGL, my aircraft encountered the wake vortices of the B-757. Three rapid full-aileron deflections were made (rightleft-right) to regain control of my aircraft. This action [was] followed by an immediate missed approach with an uneventful landing made on Runway 26. ... Tower reported wind was [from] 170 [degrees] at five knots when we reported in on the visual approach to Runway 35R.33

An ASRS follow-up interview with the captain revealed the following:

[The captain] says the most significant cause of the wake-turbulence encounter was the ATC instruction to maintain 180 knots to the marker. Initially, the separation from the B-757 was six [nautical] miles, but when [the B-757] slowed at the marker and [the captain's airplane] was [being flown at] 180 knots, the separation rapidly decreased to within [an] estimated three [nautical] miles when the encounter occurred. [The captain] also thinks the tail wind causes an aberration in the dissipation of vortices at altitude longer, rather than dissipate downward.³⁴

Pilots of Most Accident Aircraft Held Advanced Flight Certificates

Data show that 50 (38 percent) of the 130 pilots-in-command (PICs) of the accident aircraft held commercial pilot certificates, and 30 PICs (23 percent) held airline transport pilot (ATP) certificates (Table 8). Of the 50 PICs with commercial pilot certificates, 20 PICs had been cautioned

Table 8Pilot Certificate Held byPilots-in-command of Aircraft in U.S.Wake-turbulence Accidents, 1983–2000

| Type of Certificate | Number of Pilots | Number of Pilots Who Had Been Cautioned by ATC About Wake Turbulence |
|---------------------------|---------------------|---|
| Student | 14 | 7 |
| Private | 36 | 12 |
| Commercial | 50 | 20 |
| Airline transport pilot | 30 | 6 |
| Total | 130 | 45 |
| ATC = Air traffic control | | |

Source: Patrick R. Veillette, Ph.D., from U.S. National Transportation

Safety Board data on 130 accidents

about wake turbulence by ATC. Of the 30 PICs with ATP certificates, six PICs had been cautioned about wake turbulence by ATC. Pilots with private pilot certificates flew the trailing aircraft in 36 (28 percent) of the 130 accidents; 12 pilots had been cautioned about wake turbulence. Of 14 student pilots (11 percent) who flew the trailing aircraft in wake-turbulence accidents, seven pilots had been cautioned about wake turbulence.

Table 9 shows the distribution of certificates held by pilots involved in incidents in the FAA database and in events in the ASRS database. In the 60 incidents, ATPs flew 24 (40 percent) of the trailing aircraft, commercial pilots flew nine (15 percent) of the trailing aircraft, private pilots flew 20 (33 percent) of the trailing aircraft, and student pilots flew seven (12 percent) of the trailing aircraft. In the 165 events, 127 ATPs (77 percent), 26 commercial pilots (16 percent) and 12 private pilots (7 percent) flew the trailing aircraft.

Table 9Type of Pilot Certificate Held byPilots-in-command of Aircraft inU.S. Wake-turbulence Incidents,1983–2000, and Events, 1988–1999

| Type of Certificate | Number of Pilots in Incidents | Number of Pilots in Events |
|-------------------------|----------------------------------|-------------------------------|
| Student | 7 | 0 |
| Private | 20 | 12 |
| Commercial | 9 | 26 |
| Airline transport pilot | 24 | 127 |
| Total | 60 | 165 |

Source: Patrick R. Veillette, Ph.D., from U.S. Federal Aviation Administration data on 60 incidents and U.S. National Aeronautics and Space Administration Aviation Safety Reporting System data on 165 events Figure 9 shows that, of the 130 pilots of trailing aircraft involved in accidents, 37 pilots (28 percent) had more than 5,000 flight hours. Of the 60 pilots of trailing aircraft involved in incidents, 15 pilots (25 percent) had more than 5,000 flight hours, and of the 165 pilots of trailing aircraft involved in events, 107 pilots (65 percent) had more than 5,000 flight hours.

Many Pilots Described Wake-turbulence Events as 'Violent' or 'Severe'

Many of the 165 wake-turbulence events reported to the ASRS database had severe effects on the trailing aircraft. In 49 reports (30 percent), the event was described as "violent" or "severe" (Figure 10, page 28). Forty-two reports (25 percent) said that the event involved a "moderate" upset. Reports on 70 events (42 percent) said that there was a temporary loss of control; reports on 16 events (10 percent) said that pilots had refused to accept a takeoff clearance because of wake turbulence, and reports on nine events (5 percent) said that pilots rejected a takeoff because of the risk of a wake-turbulence occurrence.

The following ASRS report was filed by the pilot of an airplane identified only as a light transport aircraft:

[We were] approaching [the] airport from the northwest, following medium-large transport traffic, when the controller saw an opportunity to allow us to land on Runway 35R. We were 3,000 feet MSL [above mean sea level] at 210 knots indicated airspeed (the assigned airspeed) when told to follow the [medium-]large transport over the locator outer marker for Runway 35R. [Our airplane] crossed behind the medium-large transport on final for Runway 36L. [Our airplane was] still at 3,000 feet and intercepted the localizer for Runway 35R. [We] switched to tower frequency and were told we had a 70-knot overtake on the large transport and began slowing.

[We] began descent from 3,000 feet, noting [that] we were full deflection above glideslope. I judged this to be perfectly acceptable, knowing the nasty reputation the [medium-]large transport has for generating wake turbulence, and, in fact, [I] fully intended to remain high on final. Tower advised "cleared to land following traffic 2.5 [nautical] miles ahead, caution wake turbulence." I thought we would be safely above his wake.

Shortly thereafter, my aircraft ... rolled to the right to an angle of approximately 100 degrees (more than 90 degrees). Full opposite control input did not have any effect in stopping this roll. Indicated airspeed began dropping, and throttles were then firewalled. As we rolled right, we had also turned slightly in that direction, and I assume we flew out of that vortex and were able to right the aircraft. Then we hit what







Figure 10

I assume was [the other aircraft's] right-wing vortex, and the aircraft (mine) began to roll left. We flew through this vortex fairly quickly, probably due to our new (uncommanded) heading, and our bank did not exceed 60 degrees. We recovered from this roll on a heading of about 80 degrees and declared a missed approach. Tower asked if we could enter a base for Runway 31R and land. We did, and landed without further incident.

The large transport had obviously been very high on his approach for some reason. ... Our attention had been focused on the medium transport we were originally following; thus, I was unaware of the large transport's glide path. I feel someone (controllers) should have noticed this and realized a wake encounter was inevitable.³⁵

Figure 11 (page 29) shows the types of motion induced by flights into wake turbulence by the aircraft involved in the NTSB accidents, the FAA incidents and the ASRS events. The most common type of motion induced among the 130 accident aircraft was a rolling motion in one direction, experienced by 46 aircraft (35 percent). Veering/yawing motions were most prevalent among the 60 incident aircraft; in 17 incidents (28 percent), the aircraft experienced veering/yawing. A rolling motion in one direction was most prevalent among the 165 events; in 37 events (22 percent), the aircraft experienced primarily a rolling motion in one direction.

Compressor stalls or similar engine anomalies occurred in 12 events (7 percent) described in ASRS reports. The pilots said that the engines had ingested part of the leading aircraft's wake, resulting in a severe disturbance of inlet airflow and subsequent compressor stalls. The following ASRS report was filed by the pilot of a DC-10:

The wind was calm when we landed immediately after a heavy [Lockheed] L-1011 took off. We experienced an air burble in the flare from the jet blast. We also experienced light buffeting during rollout. Normal reverse was established ... and held until 80 knots. At 70 knots, all three engine-reverse levers were in the stowed position. At about 50 knots, two loud bangs were heard. [The] no. 1 [engine] and no. 3 engine had compressor stalls. They were shut down. [The] no. 2 engine was normal, and we taxied to the gate on one engine. Reverse and landing procedures were normal. The heavy aircraft had lifted off right about where the engines stalled. Calm winds, heavy aircraft with strong wing vortices and engines with a history of stall problems ... combined to create a problem on what should have been a normal landing.36

Severity of Wake Turbulence Determined by Many Factors

The severity of a wake-turbulence occurrence depends on many factors, including the weight and wingspan of the trailing





aircraft and the relative positions of the trailing aircraft and the wake vortices. In most of the 130 accidents, 60 incidents and 165 events, the maximum bank angle induced by wake turbulence was 30 degrees or less.

Of the 113 accidents, 46 incidents and 57 events involving small aircraft and small transport aircraft as the trailing aircraft, 81 accidents (72 percent), 25 incidents (54 percent) and 27 events (47 percent) resulted in a maximum bank angle of 30 degrees or less (Table 10, page 30).

Of the four accidents, five incidents and 17 events involving light transport aircraft as the trailing aircraft, three accidents (75 percent), four incidents (80 percent) and nine events (53 percent) resulted in a maximum bank angle of 30 degrees or less (Table 11, page 30).

Of the six accidents, four incidents and 28 events in which medium transport aircraft were the trailing aircraft, five accidents (83 percent), three incidents (75 percent) and 17 events (61 percent) resulted in a maximum bank angle of 30 degrees or less (Table 12, page 30).

Of the 25 events in which large transport aircraft were the trailing aircraft, 21 events (84 percent) resulted in a maximum bank angle of 30 degrees or less, and four events (16 percent) resulted in a maximum bank angle from 31 degrees through 60 degrees.

In the one accident and 11 events in which heavy transport aircraft were the trailing aircraft, the maximum bank angle was 30 degrees or less.

Of the 130 accidents, 60 incidents and 165 events, 14 accidents (11 percent), 10 incidents (17 percent) and nine events (5 percent) involved hard landings, which sometimes result from the sinking that accompanies an "along-track penetration between vortices" (flight between a pair of vortices) — one of three categories of wake-turbulence occurrences, according to the direction of the aircraft's entry into the vortices. (The other two categories are "along-track penetration of the vortex center" [or flight into a vortex] and "cross-track penetration" [or flight perpendicular to a pair of vortices].) In an along-track penetration between vortices, the wake vortices produce a predominant downwash (downward flow of air) and the trailing aircraft reacts as though it were entering sinking air — either with a decrease in the rate of climb, a high sink rate or a hard landing.

The downwash produced by the wake vortices of a B-727 was measured by NASA — two minutes after the airplane passed by — at 1,400 fpm, which is greater than the climb performance of some light transport aircraft. The studies calculated that after three minutes, the sink rate induced by B-727 downwash would be 1,200 fpm. The sink rate would be most severe if the trailing aircraft were at the same altitude

Table 10 Maximum Roll Angles Induced in Small Aircraft and Small Transport Aircraft in U.S. Wake-turbulence Accidents and Incidents, 1983–2000, and in Events, 1988–1999

| Roll (Bank) Angle | Accidents | Incidents | Events |
|----------------------|-----------|-----------|--------|
| (Unspecified) | 11 | 4 | 16 |
| 0–30 degrees | 81 | 25 | 27 |
| 31-60 degrees | 1 | 9 | 11 |
| 61–90 degrees | 9 | 6 | 2 |
| More than 90 degrees | 11 | 2 | 1 |
| Total | 113 | 46 | 57 |

The U.S. National Aeronautics and Space Administration (NASA) Aviation Safety Reporting System (ASRS) defines a small aircraft as weighing less than 5,000 pounds/2,300 kilograms and a small transport aircraft as weighing 5,001 pounds/2,300 kilograms to 14,500 pounds/6,600 kilograms. Numbers in kilograms have been rounded.

Source: Patrick R. Veillette, Ph.D., from U.S. National Transportation Safety Board data on 130 accidents, U.S. Federal Aviation Administration data on 60 incidents and U.S. National Aeronautics and Space Administration Aviation Safety Reporting System data on 165 events

Table 11 Maximum Roll Angles Induced in Light Transport Aircraft in U.S. Wake-turbulence Accidents and Incidents, 1983–2000, and in Events, 1988–1999

| Roll (Bank) Angle | Accidents | Incidents | Events |
|----------------------|-----------|-----------|--------|
| (Unspecified) | 0 | 0 | 2 |
| 0–30 degrees | 3 | 4 | 9 |
| 31–60 degrees | 0 | 0 | 4 |
| 61–90 degrees | 0 | 1 | 2 |
| More than 90 degrees | 1 | 0 | 0 |
| Total | 4 | 5 | 17 |

The U.S. National Aeronautics and Space Administration (NASA) Aviation Safety Reporting System (ASRS) defines a light transport aircraft as weighing 14,501 pounds/6,600 kilograms to 30,000 pounds/13,600 kilograms. Numbers in kilograms have been rounded.

Source: Patrick R. Veillette, Ph.D., from U.S. National Transportation Safety Board data on 130 accidents, U.S. Federal Aviation Administration data on 60 incidents and U.S. National Aeronautics and Space Administration Aviation Safety Reporting System data on 165 events

as the vortices. As the aircraft was forced beneath the vortices, the sink effect would be reduced. Near the ground, however, the result could be loss of control, and if a pilot were to attempt to correct the sink rate by applying back elevator, the aircraft could stall.³⁷

Of the three categories of direction of entry into vortices, an along-track penetration of the vortex center is considered the

Table 12 Maximum Roll Angles Induced in Medium Transport Aircraft in U.S. Wake-turbulence Accidents and Incidents, 1983–2000, and in Events, 1988–1999

| Roll (Bank) Angle | Accidents | Incidents | Events |
|----------------------|-----------|-----------|--------|
| (Unspecified) | 0 | 0 | 2 |
| 0–30 degrees | 5 | 3 | 17 |
| 31-60 degrees | 1 | 1 | 8 |
| 61–90 degrees | 0 | 0 | 1 |
| More than 90 degrees | 0 | 0 | 0 |
| Total | 6 | 4 | 28 |

The U.S. National Aeronautics and Space Administration (NASA) Aviation Safety Reporting System (ASRS) defines a medium transport aircraft as weighing 30,001 pounds/13,600 kilograms to 60,000 pounds/27,200 kilograms. Numbers in kilograms have been rounded.

Source: Patrick R. Veillette, Ph.D., from U.S. National Transportation Safety Board data on 130 accidents, U.S. Federal Aviation Administration data on 60 incidents and U.S. National Aeronautics and Space Administration Aviation Safety Reporting System data on 165 events

most dangerous because the trailing aircraft penetrates the vortex core and experiences a strong rolling motion.

In flight tests in which pilots attempted to fly their aircraft into the center of a wake vortex, the aircraft often were deflected or "thrown out" of the vortex, sometimes before entering the core. The deflection occurred with a rapid onset of the rolling motion, and the pilots temporarily lost control of the aircraft. In some situations, the aircraft were deflected from the wake vortex or rolled into the other wake vortex and then rolled again in the opposite direction. These reactions were common when the test aircraft was directly behind the leading aircraft and flying directly into the vortex. Test flights in which pilots attempted to fly into the vortex at a slightly skewed angle resulted in a combination of pitching and rolling, which typically deflected the aircraft away from the wake.^{38,39}

Cross-track penetrations are most frequent in the terminal area when two aircraft are in different phases of flight. The trailing aircraft crosses the wake vortices at a right angle, resulting in pitching motions and vertical loads similar to those that occur when the aircraft is flown into a wind gust. Cross-track penetration typically is short-lived and without loss of aircraft control. Nevertheless, structural failures can occur and temporary loss of control near the ground may preclude recovery of the aircraft. Of the 130 accidents in the NTSB database, the 60 incidents in the FAA database and the 165 events in the ASRS database, six accidents (5 percent) involved structural damage, and the reports describing 11 events (7 percent) said that cross-track penetrations had resulted in substantial turbulence and had increased load factors on the aircraft. Data show that small aircraft most frequently are involved as the trailing aircraft and that wake-turbulence occurrences involving small aircraft are most likely to result in bank angles of more than 30 degrees. Nevertheless, wake turbulence affects aircraft of all sizes. Researchers have recommended that the best method for pilots to avoid the risks of wake turbulence is to be aware of how wake turbulence forms.◆

Notes

- 1. The U.S. National Transportation Safety Board (NTSB) defines an accident as "an occurrence associated with the operation of an aircraft which takes place between the time any person boards the aircraft with the intention of flight and all such persons have disembarked, and in which any person suffers death or serious injury, or in which the aircraft receives substantial damage." NTSB defines an incident as "an occurrence other than an accident, associated with the operation of an aircraft, which affects or could affect the safety of operations."
- 2. NTSB defines substantial damage as "damage or failure which adversely affects the structural strength, performance, or flight characteristics of the aircraft and which would normally require major repair or replacement of the affected component. Engine failure or damage limited to an engine if only one engine fails or is damaged, bent fairings or cowling, dented skin, small punctured holes in the skin or fabric, ground damage to rotor or propeller blades, and damage to landing gear, wheels, tires, flaps, engine accessories, brakes, or wing tips are not considered 'substantial damage."
- 3. The U.S. National Aeronautics and Space Administration (NASA) Aviation Safety Reporting System (ASRS) is a confidential incident-reporting system. The ASRS Program Overview said, "Pilots, air traffic controllers, flight attendants, mechanics, ground personnel and others involved in aviation operations submit reports to the ASRS when they are involved in, or observe, an incident or situation in which aviation safety was compromised. ... ASRS de-identifies reports before entering them into the incident database. All personal and organizational names are removed. Dates, times, and related information, which could be used to infer an identity, are either generalized or eliminated."

ASRS acknowledges that its data have certain limitations. ASRS *Directline* (December 1998) said, "Reporters to ASRS may introduce biases that result from a greater tendency to report serious events than minor ones; from organizational and geographic influences; and from many other factors. All of these potential influences reduce the confidence that can be attached to statistical findings based on ASRS data. However, the proportions of consistently reported incidents to ASRS, such as altitude deviations, have been remarkably stable over many years. Therefore, users of ASRS may presume that incident reports drawn from a time interval of several or more years will reflect patterns that are broadly representative of the total universe of aviation-safety incidents of that type."

- 4. The approach-and-landing phase of flight begins when an airworthy aircraft under the control of the flight crew descends below 5,000 feet above ground level (AGL) with the intention to conduct an approach and ends when the landing is complete or the flight crew flies the aircraft above 5,000 feet AGL en route to another airport.
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Appendix Wake Turbulence Accidents and Incidents in the United States, 1983–2000

| Date | Location | Aircraft Type | Aircraft Damage | Injuries |
|--|---|--|--|--|
| Oct. 26, 2000 | Falmouth, Kentucky | Canadair CL-600 | none | 50 uninjured |
| Visual meteorolo disconnected the DFDR) showed naximum bank c eached a maxim hen increased to | ogical conditions (VMC) prevail e autopilot and manually return that the airplane rolled 10 deg of 24 degrees. During the roll, t num upward deflection of six de | as being flown over the Falmout ed. The airplane, which was in le ed the airplane to level flight. Pri grees left in 1/2 second and abo ne left aileron reached a maximu grees. Pitch attitude had been at he roll. Preliminary radar data sh e same area at 11,000 feet. | evel flight with the autopilot eliminary data from the airp out 22 degrees left in anothe um downward deflection of s bout two degrees nose up w | engaged, rolled left. The capta lane's digital flight data record er 1/2 second before reaching six degrees, and the right ailer hen the airplane entered the ro |
| Oct. 19, 2000 | Camp Springs, Maryland | Cessna 172 | substantial | 1 uninjured |
| The Cessna 172 Andrews Air Ford northerly headin vake-turbulence neared 1,600 fee | 2 was substantially damaged of ce Base. The pilot was in cont g. The pilots of each airplane advisory. As the Cessna near et, it was flown into turbulence scending in a nose-low attitude | when it was flown into wake tur act with Andrews Approach Con were advised of the location of i ed the Boeing, the Cessna pilot and rolled left. The pilot was thr e. After landing, the pilot noticed | bulence from a Boeing 72 trol. The B-727 was on fina the other airplane, and the began a climb from 1,300 fe own about the cockpit, and | 7-200 about four miles south I approach for Runway 1L, or pilot of the Cessna was given set to 1,600 feet. As the airpla when the turbulence ended, ti |
| Sept. 11, 2000 | Anchorage, Alaska | Piper PA-31-350 | substantial | 1 uninjured |
| air traffic advisor MD-11 that was o he MD-11. The p shear. The right v | the airplane toward a visual flig ries for airplanes departing th on final approach to land on Ru pilot said that after the MD-11 p | trules (VFR) reporting point, h e Lake Hood Seaplane Base. H Inway 14 at Anchorage Internatio bassed his position, his airplane ssembly separated from the airples. | He was not given an adviso onal Airport. His airplane's f entered wake turbulence the | bry about a McDonnell Dougl light path was behind and belo at produced violent vertical wi |
| ug. 20, 2000 | Tooele, Utah | Piper PA-28-181 | minor | 1 uninjured |
| epeated oscillat | ions until the airplane struck th | / 34. Near the approach end of e runway, then skidded off the run baded with fire retardant departed | unway to the right. The nose | wheel collapsed. Just before t |
| ug. 11, 2000 | Cleveland, Ohio | ATR 42-320 | none | none* |
| he airplane was | s upset by Boeing 757 wake tur | oulence at 7,000 feet and approx | imately five nautical miles (9 | 9.3 kilometers) behind the B-75 |
| une 22, 2000 | Colorado Springs, Colorado | Cessna T-41 | none | 1 uninjured |
| | Academy T-41, flown by a stud conducting a go-around above | dent pilot, entered wake turbuler the T-41. | nce from a Grumman OV-10 | experimental exhibition aircr |
| lay 20, 2000 | Cedar Rapids, Iowa | Piper PA-28-140 | minor | 1 uninjured |
| | e runway, and there was a qua | ne student pilot lost directional contractional contraction of the state of the sta | | |
| April 11, 2000 | Seattle, Washington | Cessna 172 | substantial | 1 uninjured |
| The pilot of the urbulence from a eet (1,464 mete | accident aircraft was cleared a B-767 landing on a parallel ru rs) beyond the Runway 31L th | for a touch-and-go landing on F nway. The winds were from 310 of reshold, and the runway center psed when the aircraft stopped | Runway 31R. The pilot was degrees at nine knots. The R lines were about 360 feet (| cautioned about possible wa lunway 31R threshold was 4,8 110 meters) apart. The accide |
| /larch 30, 2000 | Santa Ana, California | Gulfstream AA-5 | minor | 2 uninjured |
| • | | ed during landing. The airplane eft side of the runway, striking a | 2 | ntered wake turbulence from |
| Oct. 7, 1999 | Bay City, Texas | Air Tractor AT-502-B | substantial | 1 minor |
| evel (AGL) in a 6 | | ions flight and had completed hi nrough the wake turbulence from | | |
| Sept. 15, 1999 | Denver, Colorado | Boeing 737-500 | none | 94 uninjured |
| The crew of the 1,500 feet AGL, | Boeing 737-500 flew the airpl | ane into wake turbulence from a oting the first officer (the pilot fly | ring) to conduct a missed ap | al approach to Runway 35L. |

Appendix Wake Turbulence Accidents and Incidents in the United States, 1983–2000 (continued)

| Date | Location | Aircraft Type | Aircraft Damage | Injuries | | |
|---|--|--|--|---|--|--|
| Aug. 3, 1999 | Kenai, Alaska | Cessna 152 | substantial | 1 uninjured | | |
| direction on the sa runway into a ditc interval between o pilot of a small air | pilot was departing on Runway 19R. ame runway. According to ATC tapes, t h. U.S. Federal Aviation Administration departures of large aircraft and small a plane receives a takeoff clearance. (FA 15,600 kilograms and small aircraft as | he student pilot began her tal (FAA) Order 7110.65, <i>Air Tr</i> ircraft and that a wake-turbul A defines large aircraft as we | keoff 109 seconds later. T affic Control, said that the ence cautionary advisory eighing more than 41,000 | The aircraft veered left off the ere should be a three-minute should be issued before the | | |
| June 6, 1999 | Peachtree City, Georgia | Air Shark II | destroyed | 1 serious | | |
| | departing on Runway 13. After takeoff, th pank, and the left wing struck the ground | | to correct the roll were ur | | | |
| Jan. 15, 1999 | Plainfield, Pennsylvania | MD DC-9 | none | 1 serious, 59 uninjured | | |
| approach and sa kilometers) ahead airplane to 280 km of the turbulence attendant in the ga | The flight crew was cleared for descent from Flight Level (FL) 290 (29,000 feet) to 17,000 feet. The captain briefed the first officer on the approach and said that he would keep the airplane above a preceding Boeing 747's flight path. The B-747 was 12 nautical miles (22 kilometers) ahead and also was descending to 17,000 feet. The DC-9 captain began a 3,500-feet-per-minute descent and slowed the airplane to 280 knots. While descending through 23,500 feet, there was a moderate jolt. The captain pitched the airplane's nose up to fly out of the turbulence and asked ATC for additional separation between the two airplanes. During the wake-turbulence occurrence, a flight attendant in the galley slipped and injured her right ankle. Radar data showed that the airplane was about two minutes behind and 1,000 feet below the B-747. Winds at 23,000 feet were from 195 degrees at 90 knots. | | | | | |
| Oct. 3, 1998 | Middlebury, Connecticut | Super Cat | destroyed | 1 fatal | | |
| The pilot of the op nautical mile (1.9 | ben-cockpit airplane conducted a taked kilometers) north of the airport; the wre houlder harness, seat belts and buckle | off minutes after a Hawker 10 ckage of the airplane was fou | 00 business jet. The pilot nd in a wooded area 845 | 's body was found about one | | |
| Sept. 17, 1998 | Chicago, Illinois | ATR 42 | none | 1 serious, 15 uninjured | | |
| The Avions de Transport Regional ATR 42 was at 4,900 feet and 18 nautical miles (33 kilometers) from the airport on the instrument landing system (ILS) approach to Runway 9 when it was flown into wake turbulence from a B-737-300, which was vectored onto the approach from the north in front of the ATR 42. Radar data showed that the B-737-300 intercepted the localizer 17.5 nautical miles (32 kilometers) from the airport, while descending from 5,200 feet to 4,800 feet. Separation of the two airplanes was about 4.8 nautical miles (8.9 kilometers). Vertical acceleration of the flight varied from 2.36 g (2.36 times standard gravitational acceleration) to 0.55 g during the encounter. | | | | | | |
| Sept. 15, 1998 | Salt Lake City, Utah | Boeing 737 | none | 3 minor injuries* | | |
| | being vectored to final at 8,000 feet Three flight attendants were treated for | | turbulence from a B-76 | 7 that was three minutes 45 | | |
| Aug. 7, 1998 | McConnellsburg, Pennsylvania | Boeing 737 | minor | 10 minor, 122 uninjured | | |
| The B-737 began an uncommanded roll during climb, just before passing through 29,700 feet. The captain said that the airplane was flown into light chop, which quickly intensified. The airplane yawed slowly, then suddenly rolled right, then left. DFDR data showed that the aircraft rolled right a maximum of 37 degrees, and then within two seconds, reached the maximum left roll of 27 degrees. Vertical acceleration reached a low of minus 0.6 g. The captain recovered the aircraft and diverted to a nearby airport. The weather was clear and the air was smooth before and after the event. Radar analysis revealed that a McDonnell Douglas DC-10, about 10 nautical miles (18.5 kilometers) ahead, had climbed through the area about 600 feet higher, 71 seconds earlier. | | | | | | |
| Aug. 4, 1998 | Saint Joseph, Missouri | Cessna 140 | destroyed | 2 fatal | | |
| The pilot of the accident airplane was advised that wake turbulence would be present during the approach to Runway 35. U.S. Air Force Lockheed C-130s were being landed on Runway 31. Witnesses observed the accident airplane as it was flown toward Runway 35 at a low altitude, banked left about 35 degrees and then rapidly banked right more than 90 degrees. The airplane's right wingtip was about 20 feet above the ground when the nose dropped and the airplane struck the ground. A C-130 had been landed on Runway 31 about 10 seconds before the accident airplane reached the threshold of Runway 35. | | | | | | |
| July 17, 1998 | Olathe, Colorado | Bell 47G-3B1 | substantial | 1 uninjured | | |
| The pilot was conducting an agricultural-operations flight and had made three passes over the same path. He said that the wind increased as he turned the helicopter for a fourth pass, and the helicopter was flown into its own wake turbulence. The helicopter had insufficient power to overcome the ensuing descent and settled onto the ground in a nose-low attitude, causing the main-rotor blades to strike the tail boom and sever it from the aircraft. | | | | | | |
| April 9, 1998 | Seattle, Washington | Cessna 150 | minor | 1 minor | | |
| • | empted to land long behind a departing | | | | | |
| airplane to wings- straight ahead, a | ot rejected the landing and added full p level flight, the airplane had veered left nd the airplane became entangled in laps to 20 degrees as recommended in | t and was turned almost 90 de electrical transmission lines | egrees from the runway. T a. An investigation deter | he pilot climbed the airplane | | |
| Date | Location | Aircraft Type | Aircraft Damag | e Injuries |
|---|---|--|---|--|
| Nov. 19, 1997 | Beaumont, Texas | Cessna 310 | destroyed | 1 serious |
| The pilot said that began the taked airplane achieve | tioned the airplane on the runway, at he had the jet in sight. After the j off roll. No cautions for wake turbu d a positive rate of climb, the pilot cartwheeled, then stopped inverte | et passed, the tower cleared ilence were issued by tower retracted the landing gear, ar | the pilot of the Cessna fo personnel, and the pilot nd the airplane rolled righ | r takeoff, and the pilot immediate did not request a delay. After th it. The right wing struck the groun |
| Nov. 4, 1997 | Cleveland, Ohio | Embraer EMB-120 | none | 2 uninjured |
| | ol did not tell the crew to switch to wn into wake turbulence. | the tower radio frequency. The tower radio frequency. | he Embraer EMB-120 wa | is following a Lockheed L-1011 o |
| Oct. 21, 1997 | West Palm Beach, Florida | DA 20-A1 | substantial | 2 serious |
| McDonnell Doug airplane then rol pilot received the | at, as he flew the airplane over the glas MD-80 passed near the accide led upside down and struck the gro e clearance, the airplane was obs ne rolled left, striking the ground h | ent airplane on the right. The bund. ATC audio tapes showe erved deviating toward Runw | controller warned the pilo d that the pilot was cleare vay 27R. Controllers obse | ot of possible wake turbulence. Th ed to land on Runway 27L. After th |
| Oct. 2, 1997 | Lake Elmo, Minnesota | Beech 18-E18S | substantial | 2 uninjured |
| power. The left w struck the grass grass, where the | at the airplane lifted off at 70 knots vingtip struck the ground about thr near the left side of the departure a landing gear collapsed. Investiga an one minute before the accident | ree-quarters of the way down e end of the runway. The pilot tion revealed that another Be | i the runway. The pilot ad t then reduced power to i | ded more power, and the left win dle and landed the airplane in th |
| Aug. 15, 1997 | Newark, New Jersey | ATR 42-320 | none | 39 uninjured |
| The airplane was he airport. | s flown through wake turbulence. T | he pitch mode of the autopilo | t disconnected, and the fl | ight crew hand-flew the airplane t |
| Aug. 2, 1997 | Oshkosh, Wisconsin | Cessna 182-P | substantial | 3 uninjured |
| | a was on final approach, another h e pilot of the other airplane conduc landed hard. | | | |
| Aug. 2, 1997 | Norfolk, Nebraska | Cessna 188 | substantial | 1 uninjured |
| after arriving over The pilot of the ac the second pass | amiliar with the area, so he flew his a r the field, the pilot of the lead aircra ccident airplane circled to line up the and leveled the airplane four feet ab d. The lead airplane had been flown | ft descended to about 20 feet a airplane for a spray pattern all ove the crop. The pilot said that | AGL and flew the airplane ong the eastern edge of the at the airplane almost imme | across the field from south to north e field. He positioned the airplane for |
| July 22, 1997 | Burlington, Vermont | Piper PA-28-180 | minor | 3 uninjured |
| | s being landed behind a C-130 who knots. The airplane bounced twice | | | |
| June 19, 1997 | Richmond, Virginia | Cessna 172 | minor | 1 uninjured |
| hen a more viole | C advised caution for wake turbule ent force to the left. The pilot added the tips of the propeller. | | | |
| May 29, 1997 | Orlando, Florida | Embraer EMB-120 | none | 1 minor, 29 uninjured |
| approach. The L | being flown on approach when A -1011 was turned onto the same jured as the EMB-120 rolled sharp | heading as the EMB-120, p | placing the EMB-120 dire | |
| May 18, 1997 | Galion, Ohio | Cessna 172 | substantial | 2 uninjured |
| | nducting a takeoff from Runway 2 about 50 feet AGL, the airplane v | | | |
| March 25, 1997 | Chicago, Illinois | ATR 42-300 | none | 1 minor, 2 uninjured |
| | al miles (28 kilometers) from the DC-10 five nautical miles ahead. A | | | |
| | West Palm Beach, Florida | Cessna 172P | minor | 1 uninjured |
| Dec. 25, 1996 | West I alli Deach, I lonua | Cessila 172F | minor | i uninguiou |

| Date | Location | Aircraft Type | Aircraft Damage | Injuries |
|--|---|--|--|---|
| Nov. 30, 1996 | Santa Ana, California | MS 760 II | destroyed | 3 fatal |
| because an exter the pilot flew the a the final-approach | bilot of the Morane-Saulnier MS 760 II nal boarding ladder was still attached t irplane toward the airport, a B-757 was ocourse about one nautical mile from the red a spiral and struck a building. | o the airplane. The controller s landed on the same runway. | cleared the pilot to land Then, as the accident air | on the departure runway. As rplane was flown to intercept |
| Nov. 20, 1996 | Salt Lake City, Utah | Cessna 152 | substantial | 1 uninjured |
| Learjet had lande ends.) The airplar suddenly was blow | was cautioned about wake turbulence of d on Runway 35 about 74 seconds be ne ballooned slightly, and as the pilot a wn sideways. The winds were from 360 ded hard and rolled forward before no | efore the accident aircraft. (R applied back pressure on the degrees at 10 knots before th | unway 32 and Runway 3 control yoke to prepare | 35 intersect at the approach for touchdown, the airplane |
| Sept. 4, 1996 | Morristown, New Jersey | Cessna 182 | minor | 1 uninjured |
| | ouch-and-go landings, the pilot attemp at about 50 feet. The airplane settled o | • | 0 | |
| July 27, 1996 | Portland, Oregon | Cessna 182 | substantial | 2 minor |
| sight and complie | to expedite his approach and follow ar d with ATC instructions. The Cessna wa ane, which struck the ground. At their cl 0-80's glide path. | is flown into the MD-80's wake | e turbulence about 200 fe | et AGL on final. The pilot lost |
| July 27, 1996 | Liberal, Kansas | Air Tractor AT-301 | destroyed | 1 serious |
| | the pass on an agricultural-operations urbulence. He lost control of the airpla | | 270 degrees. The pilot s | aid that he flew the airplane |
| June 5, 1996 | Eugene, Oregon | Cessna 402 | none | 1 uninjured |
| The airplane was airplane was land | flown into wake turbulence from a landi ed normally. | ng jet, the airplane rolled, and | d the pilot recovered the a | irplane at 500 feet AGL. The |
| May 16, 1996 | Anchorage, Alaska | MD-11 | substantial | 1 minor, 1 uninjured |
| landing on Runwa beyond the thresh MD-11 rolled left | cleared for a visual approach to Runw ay 24L. The two runways are 500 feet (hold of Runway 24R. On final approac , then right, yawed slightly and enter er-aft fuselage struck the runway, and e times. | 153 meters) apart, and the th h, the 21-knot left crosswind ed a high sink rate. The cap | hreshold of Runway 24L diminished to about five tain began a go-around | is 4,300 feet (1,312 meters) knots. At 100 feet AGL, the and raised the nose of the |
| April 10, 1996 | Lakeland, Florida | Cessna 152 | minor | 1 uninjured |
| The airplane was | landed on Runway 9, then ran off the | eft side of the runway, striking | g a wingtip and damaging | g the propeller. |
| March 30, 1996 | Fullerton, California | Cessna 172 | substantial | 1 uninjured |
| The student pilot power. The left w | said that he was practicing full-stop I ingtip struck the ground, and the airp cause of the accident was the studer | andings on Runway 24. The lane struck the median betw | student pilot attempted veen the runway and the | a go-around and added full a taxiway. Investigators said |
| Sept. 30, 1995 | Avondale, Arizona | Grumman G-164B | substantial | 1 uninjured |
| this time, he spra turbulence from a | ducting an agricultural-operations fligh yed half of the field and flew the airp previous pass. The pilot pushed the co r normal recovery and the airplane str | plane in more steeply banked ontrol yoke forward to recover | d turns. During one turn | , the airplane entered wake |
| Sept. 23, 1995 | Kona, Hawaii | Cessna 150 | substantial | 1 minor |
| landings. The pilo airplane and was | nsupervised solo flight, the student pild t said that on her eighth landing, she re told to extend the downwind leg to fold he glide path of the C-130. About 10 fe | eceived ATC clearance for a s w that airplane. She was awa | stop-and-go landing behir are of the wake-turbulenc | nd a military C-130 transport e risks and planned to fly an |
| Aug. 18, 1995 | Long Beach, California | Cessna 152 | minor | 1 uninjured |
| | e, the airplane was blown to the left and turbulence of a departing jet. | d struck a visual approach slo | pe indicator (VASI) light. | The airplane had been flown |

| Date | Location | Aircraft Type | Aircraft Damage | Injuries |
|--|--|--|--|---|
| July 25, 1995 | Elyria, Ohio | Tri-Q200 | destroyed | 1 minor |
| airplane began a nour, the pilot rot | parted as a flight of two in a sta takeoff roll on the right side of ated the airplane for takeoff. We struck the ground on the left sid | the runway with a left crosswin hen the airplane was 20 feet A0 | d. When the airplane reached GL to 30 feet AGL, the left win | d 80 miles (129 kilometers) pe ng dipped. The airplane sank t |
| July 25, 1995 | New York, New York | Avro RJ70 | none | 24 uninjured |
| a preceding Airbu apply corrective a | as being flown on approach abo us A340 and rolled left. The pilo aileron input. He applied large a proach and conducted a norma | t flying, who occupied the right and/or abrupt movement of the | seat, reached for the yoke to | disconnect the autopilot and t |
| June 1, 1995 | College Station, Texas | Cessna 120 | substantial | 1 uninjured |
| at four knots. The accident airplane turbulence from t | hat the pilot was conducting a t pilot said that he had believed conducted a wheel landing, a he preceding airplane and dep the airplane nosed over to an ir | I that his airplane was two nau nd the airplane was rolling on t arted the runway to the left. The | tical miles (3.2 kilometers) be he main-landing-gear tires w | whind the Saab. The pilot of th hen the airplane entered wak |
| May 22, 1995 | Honolulu, Hawaii | Beech B18 | minor | 1 uninjured |
| The airplane rolle ncident aircraft's | ed sharply after liftoff and scrap takeoff. | ed a wingtip on the runway. The | e pilot rejected the takeoff. A l | B-737 had departed before th |
| May 3, 1995 | Redding, California | Piper PA-34-200T | minor | 2 uninjured |
| The airplane was | a landed behind a B-737 and er | ntered wake turbulence. The no | se landing gear struck the ru | nway and collapsed. |
| - eb. 23, 1995 | Elmira, California | Cessna A188 | substantial | 1 uninjured |
| nto a turn at 100 turbulence gener | gricultural-operations flight com feet AGL. The pilot said that at ated by another aircraft that had n. The right wing struck the grou | ter rolling the airplane out of a djust departed the area where | left turn and into a right turn, he was working. The wake tur | he felt the airplane enter wak |
| Jan. 1, 1995 | Houston, Texas | Boeing 737 | none | 66 uninjured |
| clean condition a | or the landing approach, the flig nd with the power reduced. The ng, the pilot applied a left corre b level attitude. | airplane was behind an MD-80 | The initial divergence was a 2 | 20-degree right roll. As the righ |
| June 29, 1994 | Newark, New Jersey | ATR 42-320 | none | 1 minor, 11 uninjured |
| Eight miles behin | nd an Airbus A300 in smooth ai | r, the ATR 42 made an abrupt 3 | 30-degree roll. A flight attenda | ant suffered a head injury. |
| lune 17, 1994 | Chicago, Illinois | MD DC-9 | none | 1 minor* |
| A flight attendant | was injured when the airplane | was flown into wake turbulenc | e from an MD-11 during cruis | se flight. |
| May 12, 1994 | Hickory, North Carolina | type unspecified | minor | none* |
| | the aircraft while another aircra | ft was departing in the opposit | e direction. The landing gear | collapsed. |
| April 23, 1994 | Santa Monica, California | Fairchild SA-227 | minor | 1 minor, 19 uninjured |
| The airplane was B-747-400 five na | s at 7,100 feet approaching Lo autical miles ahead. The airplar uring recovery from the invertee | s Angeles (California) Internati ne rolled left. The first officer ap | onal Airport when it was flow plied full right aileron, but the | n into wake turbulence from airplane continued to roll un |
| Dec. 15, 1993 | Santa Ana, California | IAI 1124A | destroyed | 5 fatal |
| Before receiving a course. Crews of final approach an on a three-degree Westwind captair B-757. While des | srael Aircraft Industries 1124A ATC clearance for the visual app the B-757 and the Westwind we id descending on a 5.6-degree e approach. ATC did not tell (an- n discussed possible wake turbu cending through 1,100 feet, the crew had not received training t | proach, the Westwind was 3.5 n ere told to slow to 150 knots. The glide path. The Westwind conve d at the time was not required to ulence, flew the airplane one do Westwind entered wake turbu | autical miles (6.5 kilometers) f ne B-757 was slowed to less th erged to 2.1 nautical miles (3. o tell), the Westwind crew that of high on the glideslope and v lence from the B-757, rolled in | from the B-757 on a convergin han 150 knots and was high o 9 kilometers) behind the B-75 they were behind a B-757. Th vas aware of the location of th |

| Date | Location | Aircraft Type | Aircraft Damage | Injuries |
|---|--|--|--|---|
| Nov. 9, 1993 | Salt Lake City, Utah | Cessna 182R | destroyed | 1 minor, 2 uninjured |
| Runway 35 and t he crew of a B- additional Boein airplane on the e lew into slight w | d ATC clearance into the traffic pate to land the airplane on Runway 32. 757 was cleared to land on Runw g traffic on a one-nautical-mile fin- extended centerline for Runway 32 vake turbulence, and the pilot add up, rolled right and struck the grou | ATC requested that the pilot ay 35 and was advised of the al and that he should fly the over the threshold of Runway led power because he expect | make a left 360-degree tur e Cessna traffic. ATC told t airplane to the numbers or / 35 and prepared for a lan | n. After the turn was completed the Cessna pilot that there wa n Runway 32. The pilot flew the ding with full flaps. The airplan |
| Oct. 15, 1993 | Colorado Springs, Colorado | Cessna 172 | substantial | 1 uninjured |
| | t was on his first solo flight and v Runway 17R. As the student pilot b | | | |
| Sept. 22, 1993 | Surprise, Arizona | Rockwell S2-600 | substantial | 1 minor |
| | ere being flown on agricultural-ope during a turn-around maneuver at | | | as flown into the other airplane' |
| Sept. 14, 1993 | Reno, Nevada | R&K Special 01 | destroyed | 1 serious |
| said that, after se – about 50 feet. | ng his homebuilt experimental bipla everal laps at a higher altitude, the He flew the airplane around pylon n immediate pitch down. The airpla | pilot flew the airplane to the s s and was flying down the eas | same lower altitude that pre | evious pilots had used to qualif |
| July 31, 1993 | Anchorage, Alaska | Piper PA-18 | substantial | 1 minor |
| airplane was flow | ndown, the floatplane's wings rocke vn into the wake turbulence from a distance behind the Beaver, but a er. | de Havilland DHC-2 Beaver th | nat had been landed second | ds earlier. The pilot said that sh |
| luly 30, 1993 | Verdi, Nevada | Robinson R22 | substantial | 2 uninjured |
| nstructor allowe nelicopter's wake per minute begai | as one of four helicopters being fluid the student pilot to follow anothe turbulence and immediately turned n to decrease. The flight instructor flight instructor returned the helico | r helicopter on departure from d right. The student pilot applie took the controls, lowered the | n the pinnacle. The helicop ed left-pedal corrective actic collective and applied full t | ter was flown into the precedin on, but the main-rotor revolution hrottle, but the rear skids struc |
| luly 24, 1993 | Vacaville, California | Cessna 172 | substantial | 4 uninjured |
| oossible wake tu around. During t | d ATC clearance to conduct a stra irbulence. While nearing the runw he go-around, the airplane was flo ne runway and skidded to a stop. | ay threshold, the airplane wa | as flown into wake turbuler | nce and the pilot initiated a go |
| lune 2, 1993 | Walnut Ridge, Arkansas | Grumman G-164B | minor | 1 uninjured |
| he agricultural- hen was landed | operations airplane was flown thro safely. | ough its own wake turbulence | e, and both main landing ge | ear struck a levee. The airplan |
| April 23, 1993 | Denver, Colorado | Boeing 737-522 | none | 133 uninjured |
| The crew correct approach to Run neters) east of F nautical miles (2 glide path of Ru | oach to Runway 26L, the flight cre ted the roll and conducted a go-a way 26R. The two runways were 6 Runway 26R. The wind at the onset .5 kilometers), or 32 seconds, apa nway 26L. Weather data showed y (a boundary between two small a | around and a normal landing 00 feet (183 meters) apart, ar of the incident was from the r art. The B-757 wake vortices evidence of possible interact | . The B-737 was behind a nd the threshold for Runway orthwest at five knots to 10 had settled about 100 feet ion between the wake turk | B-757, which was on a visua 26L was about 1,300 feet (39 knots. The two aircraft were 1. and moved laterally toward th |
| March 1, 1993 | Orlando, Florida | MD-88 | no damage | none* |
| The crew of the The crew of the udder pedal to c ight-wing down. | McDonnell Douglas MD-88 was MD-88 said that the airplane sud- correct the uncommanded roll. Dat The crew regained control and c ut 2.5 nautical miles (4.6 kilomete | conducting a visual approac denly rolled right about 15 de a from the DFDR indicate tha onducted a normal landing. | h to Runway 18R while fo egrees, and the pilot rapidl t at about 110 feet AGL, the Recorded radar data show | llowing a B-757 to the airport y deflected both the wheel and e roll angle reached 13 degree / that at the point of upset, the |

| Date | Location | Aircraft Type | Aircraft Damage | Injuries |
|--|---|---|---|---|
| Dec. 18, 1992 | Billings, Montana | Cessna 550 | destroyed | 8 fatal |
| About 1.5 nautic descend almost visual awarenes was 600 feet to | al miles (2.8 kilometers) from vertically into the ground. ATC s of the position of the B-757 | ehind a B-757, and the crews of b the runway, the accident airplane C transcripts and the airplane's co throughout the approach. At the aration was decreasing below 2.6 | e was observed to roll rapidly ockpit voice recorder reveale time of the upset, vertical se | / to the inverted position and to d that the crew had maintained paration between the airplane |
| Nov. 11, 1992 | Los Angeles, California | Boeing 737-322 | none | none* |
| The airplane wa | s on approach when it rolled r | ight because of wake turbulence | . The airplane was landed sa | ifely. |
| Oct. 27, 1992 | Saipan, Northern Mariana | Islands Cessna 310 | destroyed | 3 fatal |
| runway about th AGL and bankee | e same time a DC-10 was liftir | an its takeoff from an intersection ng off the ground. They said that t a about 30 degrees right and thei truck the runway inverted. | the accident airplane was flow | wn to about 200 feet to 250 fee |
| Oct. 24, 1992 | Apopka, Florida | Velocity | substantial | 1 fatal |
| The pilots were a experimental air to descend. The 9,500 feet. Abou | advised of each other's positio plane but being flown higher a B-727 passed over the expe | eing flown in controlled airspace i n and heading. Both airplanes we nd to the left. The pilots of the B-7 rimental airplane at 10,000 feet, of the experimental airplane told A o wash — the vortex." | re on a southeasterly heading 727 were told to maintain visu as the experimental airplan | g, with the B-727 overtaking th Ial separation and were cleare e's pilot began a descent fror |
| July 7, 1992 | Okeechobee, Florida | Maule MX-7-180 | substantial | 1 minor |
| operations that I Route 34, the Ma | he planned to fly his airplane aule was flown near a flight of t | btain notices to airmen about his south of the restricted area at Av four F-16 aircraft at 1,500 feet. Th I a collision with the Maule, which | /on Park. While in cruise fligh e F-16s were being flown at 5 | nt at 1,400 feet over Instrumer 500 knots in wide formation. Th |
| June 2, 1992 | Delaware, Ohio | Beech B35 | substantial | 1 minor |
| AGL, and the air pounds (3,810 k continued acros | plane pilot planned a touchdov (ilograms), touched down, the | S helicopter on approach to landi vn 1,500 feet (458 meters) from th airplane crossed the threshold a aircraft parking area. The airplan | ne approach end. Before the h and rolled left. The left wing s | nelicopter, which weighed 8,40 struck the ground. The airplan |
| April 22, 1992 | Austin, Texas | Cessna 310P | substantial | 2 uninjured |
| A military transp approach and he said, "Separation that her airplane | overed the helicopter at 300 fe n should be just fine." Soon afte was supposed to be behind nd we were one-three right." A | approach to Runway 13R aheac eet over the runway. The pilot of i rrward, as the airplane was over th the helicopter. ATC said, "You we is the airplane was being flared, | the accident airplane reques he threshold of Runway 13R, ere cleared to land on the lef | e helicopter pilot terminated th ted vectors for separation; AT the pilot requested confirmatio t runway." The pilot responded |
| Feb. 28, 1992 | Anaheim, California | Beech 90 | none | 1 minor, 3 uninjured |
| The airplane wa | s flown into wake turbulence v | when a B-737 crossed its path. A | passenger whose seat belt | was not fastened was hurt. |
| Nov. 20, 1991 | Chicago, Illinois | ATR 42 | none | 1 minor, 21 uninjured |
| minor injuries. R the first airplane | adar data show that a similar of was descended to the same a | while the flight crew was complyin category airplane was four nautica ltitude as the incident airplane and le ATR 42 was flown into the wak | al miles (7.4 kilometers) in fro d remained at that altitude. Th | nt of the incident airplane whe |
| Sept. 13, 1991 | Prescott, Arizona | Cessna 172N | substantial | 1 uninjured |
| on a 7,616-foot runway. The priv | by 150-foot (2,323-meter by vate pilot said that the airplane | 9 hours total time and 3.7 hours a 46-meter) runway. About 30 sec 9 shook during the takeoff roll an 9 runway and collided with a dirt t | onds earlier, a Beech 1900 I Id that he applied brakes and | had been flown from the sam |
| Sept. 7, 1991 | Marion, Ohio | S-7 Courier | substantial | 1 serious, 1 minor |
| • | xperimental airplane conducte | | | |

| Date | Location | Aircraft Type | Aircraft Damage | Injuries |
|---|---|--|--|--|
| Aug. 17, 1991 | Seagraves, Texas | Piper PA-25-150 | destroyed | 1 minor |
| | nducting a formation agricultural-opera craft. The altitude was insufficient for re | | the airplane when it was | s flown into wake turbulence |
| June 28, 1991 | Clinton, Minnesota | Piper PA-25-235 | destroyed | 1 uninjured |
| see the marker fla | nducting a tandem agricultural-operatic ag in time to make a proper pass. He co raight-and-level flight when he flew into | nducted a go-around and re-e | ntered a left pattern for th | e field. The pilot said that his |
| June 20, 1991 | Salt Lake City, Utah | Cessna 210 | substantial | 2 uninjured |
| The airplane was The airplane lanc | being flared to land when it passed thro led hard. | ough wake turbulence generat | ed by a helicopter that wa | as taking off near the runway. |
| March 16, 1991 | Pullman, Washington | Cessna 140 | substantial | 1 uninjured |
| | essna 140 said that his airplane was flo uter aircraft was landed. The accident a | | | |
| March 11, 1991 | Santa Ana, California | Cessna 152 | destroyed | 1 uninjured |
| B-757 that was be | nducting a fourth touch-and-go landing bing landed just ahead of the accident a nway. A post-accident fire destroyed th | airplane on Runway 19R. The a | airplane was being flared | when it suddenly rolled right |
| Feb. 4, 1991 | Greensboro, North Carolina | Piper PA-28-180 | substantial | 1 minor |
| on Runway 23 ab | who was disoriented and off course, o bout 100 feet (31 meters) behind a Mc urbulence and struck the runway. | | • | |
| Jan. 21, 1991 | Sacramento, California | Cessna 172 | destroyed | 1 serious |
| turned west, desc flight path of the | radar tracked the accident airplane as cended to 800 feet and crossed the exter MD-80 one nautical mile behind the tr ved the lights of the Cessna pass behind | ended centerline of Runway 34 ansport airplane and 100 feet | L behind an arriving MD- below, then abruptly dis | 80. The airplane crossed the sappeared from radar. Tower |
| Jan. 12, 1991 | Camarillo, California | Quickie | substantial | 1 uninjured |
| | ng the experimental aircraft on final ap 0 feet above the ground, the aircraft er | | | |
| Sept. 16, 1990 | Poteet, Texas | Cessna 188 | minor | 1 uninjured |
| | perations airplane took off with a full lo n emergency landing. | ad in high temperatures and v | vas flown into wake turbu | lence during the takeoff. The |
| July 14, 1990 | Seattle, Washington | North American P-51 | substantial | 1 uninjured |
| rolled 70 degrees | ered wake turbulence while being flown to 75 degrees left. The pilot had insuff egrees of bank, damaging the left wing | ficient control authority to reco | over. The airplane struck | |
| June 28, 1990 | Ojai, California | Bellanca 17-30A | none | 1 minor |
| westbound Bellar to 300 feet (91 m | S. Navy Grumman F-14 had received on the awas in level flight at 8,500 feet. The eters) of each other and abruptly climb in into the F-14's wake turbulence. | F-14 pilot observed the Bellar | nca when the aircraft wer | e within 100 feet (31 meters) |
| June 28, 1990 | New York, New York | Beech 1900 | none | 13 uninjured |
| The airplane ente | ered wake turbulence on landing and w | as moved sideways. Two of th | e airplane's tires failed. | |
| June 2, 1990 | Rialto, California | Cessna 152 | substantial | 2 minor |
| | nducting the initial climb after takeoff v icopter's wake turbulence, and the pilo | | opter hovering near a tax | iway. The airplane then was |
| May 31, 1990 | Anchorage, Alaska | Cessna 195 | substantial | 3 uninjured |
| | he airplane close behind a departing B al for wake turbulence. | -757 and subsequently lost di | rectional control. He had | been cautioned by the tower |

| Date | Location | Aircraft Type | Aircraft Damage | Injuries |
|--------------------------------------|--|--|--|--|
| May 6, 1990 | Windsor Locks, Connecticut | Cessna 172N | minor | 2 uninjured |
| The pilot lost co | ntrol of the airplane during landing | . The airplane was flown into | wake turbulence, veered and | d struck runway lights. |
| April 1, 1990 | Westfield, Massachusetts | Mustang 2 | substantial | 2 uninjured |
| off, it was obser | experimental airplane began a take ved to roll 90 degrees right, then 1 trees ahead, so he rejected the tak | 80 degrees left and then wir | ngs-level. The pilot said that I | he did not believe the airplane |
| March 9, 1990 | Austin, Texas | Beech 95 | minor | none* |
| The airplane en | tered wake turbulence during landi | ng and bounced during rollou | ut. The nosewheel and lower | strut broke. |
| Jan. 20, 1990 | Scottsdale, Arizona | Boeing B75 | none | 1 uninjured |
| The airplane en | tered wake turbulence during landi | ng and veered off the runway | Ι. | |
| Dec. 3, 1989 | Houston, Texas | Embraer EMB-120 | none | 1 serious, 15 uninjured |
| During final app | roach, the airplane was flown into | wake turbulence, and a flight | attendant struck the ceiling. | |
| Oct. 5, 1989 | Palm Springs, California | Piper PA-28RT-201 | destroyed | 4 fatal |
| land on the sam a close downwir | s flown into the left traffic pattern fo e runway. ATC issued an advisory fo nd when the B-727 was landed. The nding turn. At 100 feet AGL to 200 | or wake turbulence. The accid e pilot of the accident airplan | ent airplane was abeam the a e received clearance to land | approach end of the runway o I. The airplane entered a stee |
| Oct. 1, 1989 | West Palm Beach, Florida | Piper PA-38-112 | minor | 2 uninjured |
| During takeoff, t unway lights. | he airplane was flown into wake turl | oulence from a departing airc | raft. The pilot lost directional o | control, and the airplane struc |
| Sept. 26, 1989 | Portland, Oregon | Piper PA-32-260 | substantial | 1 serious |
| airplane. The pil | ed ATC clearance to land and was ot was told to fly the airplane in a ti rbulence of the large airplane. The | ght pattern and follow the lar | ge airplane. On short final, th | ne accident airplane was flow |
| Sept. 14, 1989 | Santa Paula, California | Cessna 152 | substantial | 1 uninjured |
| | t was practicing landings in calm w wn into wake turbulence and abrup | | | |
| Sept. 6, 1989 | Santa Ana, California | Cessna 180 | substantial | 1 uninjured |
| | te before the accident, the pilot want of the pilot want of the struck the runway, and | | wake turbulence from a B-7 | 37 departing on Runway 19I |
| July 31, 1989 | Oshkosh, Wisconsin | Cessna 210K | minor | 1 uninjured |
| The airplane wastruck a taxiway | s flown into wake turbulence during light. | landing. The right wing lowe | red, and the airplane turned i | right, departed the runway an |
| lune 18, 1989 | Port Huron, Michigan | Cessna 150 | destroyed | 1 serious |
| 0.46 kilometer) | t was flying the airplane on approac behind the JU-52, which touched c ide to side and struck the ground. | | | |
| June 14, 1989 | Columbus, Ohio | Gulfstream AA-5 | destroyed | 1 minor, 3 uninjured |
| B-737. The airpl struck an airpor | d instructor were on a night instrur ane entered wake turbulence. The t ramp area. The aircraft stopped b d the runway threshold 38 seconds | flight instructor began a go-a beneath the wingtip of a park | round, but the airplane agair | n entered wake turbulence an |
| May 23, 1989 | Phoenix, Arizona | Piper PA-32RT-300T | substantial | 1 uninjured |
| could see the B runway. The pilo | s being flown on a night VFR appro -737 throughout the approach and t of the accident airplane was warr shold, the pilot felt turbulence and i | d landing. When the acciden ted of possible wake turbulen | t airplane was on base leg, ce and received clearance to | the B-737 was turning off th and. As the airplane crosse |
| May 2, 1989 | Philadelphia, Pennsylvania | Cessna T-210N | none | 1 uninjured |
| - | | | e right wingtip struck the run | • |

| Date | Location | Aircraft Type | Aircraft Damage | e Injuries |
|---|--|---|--|--|
| March 22, 1989 | | Piper PA-60-600 | destroyed | 1 fatal |
| Irizzle and fog. H airplane descene | le was told that a DC-9 was four n ded below the ILS glideslope, stru | ay 7 approach during dark-night c autical miles ahead and that he sh uck trees and then struck terrain a rtation Safety Board showed that | nould use caution for wak about 1.8 nautical miles (| e turbulence. On final approach, th 3.3 kilometers) short of the runwa |
| eb. 3, 1989 | Key West, Florida | Waco YMF | substantial | 3 minor |
| n the area at ab | a b c c | ght over the water at about 100 fe dent. The pilot reversed course to sank. | • | |
| an. 19, 1989 | Phoenix, Arizona | Piper PA-28-235 | minor | 1 uninjured |
| he airplane wa | s flown into wake turbulence du | ring landing. The right wingtip str | ruck the runway, resultin | g in a fuel leak. |
| Dec. 31, 1988 | Grand Rapids, Michigan | Cessna 152 | destroyed | 1 uninjured |
| The student pilo | t was attempting to land the airpl | ane when the airplane was flown ne, which struck the runway and | i into wake turbulence fro | m a preceding B-727. The stude |
| lov. 19, 1988 | Van Nuys, California | Piper PA-28R-201T | substantial | 1 minor |
| The pilot lost con airplane behind ight bank and tu | ntrol of the airplane while descer a Beech King Air on Runway 16F | nding for landing, and the airplane R. The pilot said that at 50 feet AG ng area. The airplane then struck nds behind the landing King Air. | L, near the threshold, th | e airplane entered an uncontrolle |
| Nov. 15, 1988 | Harkers Island, North Carolin | a Cessna 152 | destroyed | 1 serious |
| The pilot was or hat a wider orb | biting the airplane over a school | of fish at 800 feet AGL when the n flying the airplane back into th | e airplane was flown into | |
| onducting a low urbulence from | w approach to Runway 10. The the P-3. The pilot conducted the | Cessna 152 as told by ATC to taxi to Runway pilot of the accident airplane rec takeoff, and at 100 feet, the airpla scuss takeoffs behind aircraft the | eived a takeoff clearanc ane abruptly rolled right, | e and was cautioned about wak descended and struck the runwa |
| rom right to left naintain visual o vas from 250 do howed that the he B-727 and b bath, an abrupt a but the airplane | . He was cautioned about wake contact with the B-727. The pilot re egrees at five knots — a direction crew of the B-727 conducted a st elow its approach path. At about altitude deviation occurred. The p again was flown about 200 feet b | Cessna 210 in approach to Runway 02R and v turbulence and replied, "OK, I se ecceived clearance to land on Runv on that meant wake vortices from raight descent to Runway 02L and 1,100 feet AGL, when the accide ilot reported entering the wake- | ee him." The controller to vay 02R but was not given Runway 02L would drif d that accident airplane w nt airplane was about 20 Irbulence but continued in | Id the pilot to turn inbound and n information about the wind, whic t toward Runway 02R. Radar da ras about two nautical miles behir 0 feet below the B-727's approace |
| | | steep descent about one nautical threshold is 1,800 feet (549 mete | mile from Runway 02L. | st report of wake turbulence, rad The centerlines of the two runway |
| re 1,650 feet (5 | | steep descent about one nautical | mile from Runway 02L. | st report of wake turbulence, rad The centerlines of the two runway |
| re 1,650 feet (5 Oct. 27, 1988 The airplane wa | 03 meters) apart; Runway 02L's El Paso, Texas | steep descent about one nautical threshold is 1,800 feet (549 mete Maule M-6-235 ring landing. The pilot lost contro | mile from Runway 02L. rs) beyond the threshold minor | st report of wake turbulence, rad The centerlines of the two runway of Runway 02R. 1 uninjured |
| re 1,650 feet (5 Oct. 27, 1988 The airplane wa The airplane to g | 03 meters) apart; Runway 02L's El Paso, Texas s flown into wake turbulence du | steep descent about one nautical threshold is 1,800 feet (549 mete Maule M-6-235 ring landing. The pilot lost contro | mile from Runway 02L. rs) beyond the threshold minor | st report of wake turbulence, rad The centerlines of the two runway of Runway 02R. 1 uninjured |
| re 1,650 feet (5 oct. 27, 1988 'he airplane wa he airplane to g sept. 14, 1988 'he airplane wa | 03 meters) apart; Runway 02L's El Paso, Texas s flown into wake turbulence du ground-loop. The pilot had been a Orlando, Florida | steep descent about one nautical threshold is 1,800 feet (549 mete Maule M-6-235 ring landing. The pilot lost contro advised about wake turbulence. | mile from Runway 02L. ors) beyond the threshold minor of of the airplane, and a w minor | st report of wake turbulence, rad The centerlines of the two runway of Runway 02R. 1 uninjured vingtip struck the runway, causir 11 uninjured |
| rre 1,650 feet (5 Dct. 27, 1988 The airplane wa he airplane to g Sept. 14, 1988 The airplane wa vere damaged. | 03 meters) apart; Runway 02L's El Paso, Texas s flown into wake turbulence du ground-loop. The pilot had been a Orlando, Florida | steep descent about one nautical threshold is 1,800 feet (549 mete Maule M-6-235 ring landing. The pilot lost contro advised about wake turbulence. Embraer EMB-110 | mile from Runway 02L. ors) beyond the threshold minor of of the airplane, and a w minor | st report of wake turbulence, rad The centerlines of the two runway of Runway 02R. 1 uninjured vingtip struck the runway, causir 11 uninjured |
| re 1,650 feet (5 Dct. 27, 1988 The airplane wa he airplane to g Sept. 14, 1988 The airplane wa vere damaged. uly 18, 1988 The pilot was co is airplane in a s own wake tur | i03 meters) apart; Runway 02L's El Paso, Texas s flown into wake turbulence du ground-loop. The pilot had been a Orlando, Florida is flown into wake turbulence du Cape Girardeau, Missouri nducting an agricultural-operatio circle around one tower, then fle bulence. The airplane banked rig | steep descent about one nautical threshold is 1,800 feet (549 mete Maule M-6-235 ring landing. The pilot lost contro advised about wake turbulence. Embraer EMB-110 ring landing. A loud noise was h | mile from Runway 02L. rs) beyond the threshold minor of the airplane, and a w minor neard during recovery, a substantial io transmission towers a the field. At the end of the s, damaging the right win | st report of wake turbulence, rad The centerlines of the two runway of Runway 02R. 1 uninjured wingtip struck the runway, causir 11 uninjured nd a landing-gear door and hing 1 uninjured long one side. He said that he fle e pass, the airplane was flown in gtips and propeller. The wire stril |
| are 1,650 feet (5 Dct. 27, 1988 The airplane wa he airplane to g Sept. 14, 1988 The airplane wa vere damaged. July 18, 1988 The pilot was co his airplane in a ts own wake tur | i03 meters) apart; Runway 02L's El Paso, Texas s flown into wake turbulence du ground-loop. The pilot had been a Orlando, Florida is flown into wake turbulence du Cape Girardeau, Missouri nducting an agricultural-operatio circle around one tower, then fle bulence. The airplane banked rig | steep descent about one nautical threshold is 1,800 feet (549 mete Maule M-6-235 ring landing. The pilot lost contro advised about wake turbulence. Embraer EMB-110 uring landing. A loud noise was h Grumman G164-A ons flight on a field with three radi w a final pass across the end of t ht and collided with two guy wires | mile from Runway 02L. rs) beyond the threshold minor of the airplane, and a w minor neard during recovery, a substantial io transmission towers a the field. At the end of the s, damaging the right win | st report of wake turbulence, rad. The centerlines of the two runway of Runway 02R. 1 uninjured wingtip struck the runway, causir 11 uninjured nd a landing-gear door and hing 1 uninjured long one side. He said that he fle e pass, the airplane was flown in gtips and propeller. The wire strik |
| re 1,650 feet (5 Oct. 27, 1988 The airplane wa he airplane to g Sept. 14, 1988 The airplane wa vere damaged. uly 18, 1988 The pilot was co is airplane in a so own wake tur lamaged the ail une 7, 1988 During an agricu | 03 meters) apart; Runway 02L's El Paso, Texas s flown into wake turbulence du ground-loop. The pilot had been Orlando, Florida as flown into wake turbulence du Cape Girardeau, Missouri nducting an agricultural-operatio circle around one tower, then fle bulence. The airplane banked rig eron system, and the pilot cond Hazen, Arkansas ultural-operations flight at dawn, | steep descent about one nautical threshold is 1,800 feet (549 mete Maule M-6-235 ring landing. The pilot lost contro advised about wake turbulence. Embraer EMB-110 uring landing. A loud noise was h Grumman G164-A ons flight on a field with three radi th and collided with two guy wires ucted a power-off emergency lar | mile from Runway 02L. rs) beyond the threshold minor of the airplane, and a w minor neard during recovery, a substantial io transmission towers a the field. At the end of the s, damaging the right win nding in a cornfield, whe substantial turbulence and struck a | st report of wake turbulence, rad The centerlines of the two runway of Runway 02R. 1 uninjured wingtip struck the runway, causir 11 uninjured nd a landing-gear door and hing 1 uninjured long one side. He said that he fle e pass, the airplane was flown in gtips and propeller. The wire strik re the airplane nosed over. 1 uninjured |
| Are 1,650 feet (5 Oct. 27, 1988 The airplane was the airplane to g Sept. 14, 1988 The airplane was vere damaged. Inly 18, 1988 The pilot was co is airplane in a ts own wake tur lamaged the ail June 7, 1988 During an agricu | 03 meters) apart; Runway 02L's El Paso, Texas s flown into wake turbulence du ground-loop. The pilot had been Orlando, Florida as flown into wake turbulence du Cape Girardeau, Missouri nducting an agricultural-operatio circle around one tower, then fle bulence. The airplane banked rig eron system, and the pilot cond Hazen, Arkansas ultural-operations flight at dawn, | steep descent about one nautical threshold is 1,800 feet (549 mete Maule M-6-235 ring landing. The pilot lost contro advised about wake turbulence. Embraer EMB-110 uring landing. A loud noise was h Grumman G164-A ons flight on a field with three radi th and collided with two guy wires ucted a power-off emergency lar Grumman G164-B the airplane was flown into wake | mile from Runway 02L. rs) beyond the threshold minor of the airplane, and a w minor neard during recovery, a substantial io transmission towers a the field. At the end of the s, damaging the right win nding in a cornfield, whe substantial turbulence and struck a | st report of wake turbulence, rac The centerlines of the two runwa of Runway 02R. 1 uninjured wingtip struck the runway, causi 11 uninjured nd a landing-gear door and hin 1 uninjured long one side. He said that he fle e pass, the airplane was flown ir gtips and propeller. The wire stri re the airplane nosed over. 1 uninjured |

| Date | Location | Aircraft Type | Aircraft Damage | Injuries |
|---|--|--|---|---|
| | n with other aircraft in an agricultu e right wingtip struck terrain, and t | | | |
| Feb. 2, 1988 | Saint Louis, Missouri | Beech B18 | none | 1 uninjured |
| The airplane wa | as landed into wake turbulence be | hind a B-737. The pilot lost co | ontrol of the airplane, which v | veered off the runway into muc |
| Jan. 26, 1988 | El Toro, California | Cessna 152 | destroyed | 1 uninjured |
| C-130's touchdo airplane was flo | ot was practicing touch-and-go lar own point and planned his approa wn into wake turbulence from the ne runway revealed that the Cessi | ch to remain above the C-130 C-130. The airplane landed h | D's flight path. Just before lan ard, and the nose landing gea | ding, at about 10 feet AGL, th ar collapsed. An examination of |
| Jan. 9, 1988 | Colorado Springs, Colorado | Rotorway Executive | destroyed | 1 uninjured |
| A, which paralle three knots to fi lifted off about passed the helio | ed ATC clearance to taxi the helico eled Runway 17/35 and was 400 fe ve knots when the crew of a U.S. 500 feet to 1,000 feet (153 meters copter. The helicopter entered wak buched down hard. | eet (122 meters) west. The pil Air Force Lockheed C-141 co to 305 meters) ahead of the | lot was hover-taxiing the heli onducted a touch-and-go land helicopter and was at 50 fee | copter just above the ground a ding on Runway 17. The C-14 at AGL to 100 feet AGL when |
| Dec. 9, 1987 | Anchorage, Alaska | Cessna 402B | substantial | 2 minor, 3 uninjured |
| Runway 06L. AT As the accident flown into wake descended and drifted from Rur | heavy traffic, the crew of the acci C told the crew of the accident airpl airplane crossed the threshold of turbulence and rolled right more struck the ground. ATC had not tway 06L to Runway 06R in 28 se s 4,600 feet (1,403 meters) beyond | ane that the winds at the appro Runway 06R at about 100 fee than 90 degrees. The pilot at issued a wake-turbulence ac conds. Centerlines of the two | ach end of Runway 06R were t AGL (69 seconds after the E ttempted to correct with ailen lvisory. Calculations showed runways were 700 feet (214 | from 340 degrees at nine knot: 3-727 landed), the airplane wa on and power, but the airplan that wake vortices could hav |
| | | Deeeb 05 | | |
| Sept. 8, 1987 | Monterey, California | Beech 95 | destroyed | 3 fatal |
| A commercial p Runway 10 app observed the B | Monterey, California ilot was receiving multi-engine dua roach, the airplane was flown into sech in a steep nose-down descer e-out approach when the airplane | al instruction. After takeoff, the o the left traffic pattern for Ru nt. The configuration of the ai | e pilot began practicing instru nway 28, following a British / | iment approaches. After an IL Aerospace BAe 146. A witnes |
| A commercial p Runway 10 app observed the B simulated engin | ilot was receiving multi-engine dua roach, the airplane was flown into eech in a steep nose-down descei | al instruction. After takeoff, the o the left traffic pattern for Ru nt. The configuration of the ai | e pilot began practicing instru nway 28, following a British / | iment approaches. After an IL Aerospace BAe 146. A witnes |
| A commercial p Runway 10 app observed the B simulated engin Sept. 8, 1987 The pilot of the a observation pas The helicopter w | ilot was receiving multi-engine dua roach, the airplane was flown into eech in a steep nose-down descei e-out approach when the airplane | al instruction. After takeoff, the o the left traffic pattern for Ru nt. The configuration of the ai e entered wake turbulence. Bell 47-G4A cted a takeoff from a truck with r a spraying run in the opposite nce and began to settle, and th | e pilot began practicing instru nway 28, following a British rplane indicated that the pilot substantial winds from the northeast at for e direction. He was unaware o ne pilot increased collective to | Arene approaches. After an IL Aerospace BAe 146. A witnes is may have been conducting 1 uninjured bur knots to six knots. He flew a f the wind shift to the northwes stop the descent. He attempte |
| A commercial p Runway 10 app observed the Bu simulated engin Sept. 8, 1987 The pilot of the a observation pas The helicopter w | ilot was receiving multi-engine dua roach, the airplane was flown into eech in a steep nose-down descer e-out approach when the airplane Minot, North Dakota agricultural-operations flight conduc s, then began a descending turn fo vas flown into its own wake turbuler | al instruction. After takeoff, the o the left traffic pattern for Ru nt. The configuration of the ai e entered wake turbulence. Bell 47-G4A cted a takeoff from a truck with r a spraying run in the opposite nce and began to settle, and th | e pilot began practicing instru nway 28, following a British rplane indicated that the pilot substantial winds from the northeast at for e direction. He was unaware o ne pilot increased collective to | Arene approaches. After an IL Aerospace BAe 146. A witnes is may have been conducting 1 uninjured bur knots to six knots. He flew a f the wind shift to the northwes stop the descent. He attempte |
| A commercial p Runway 10 app observed the Bo simulated engin Sept. 8, 1987 The pilot of the a observation pas The helicopter w or release the lo Aug. 26, 1987 The airplane was ground in a corn | ilot was receiving multi-engine dua roach, the airplane was flown into eech in a steep nose-down descer- e-out approach when the airplane Minot, North Dakota agricultural-operations flight conduc s, then began a descending turn fo vas flown into its own wake turbuler ad of chemicals, but the dump value | al instruction. After takeoff, the o the left traffic pattern for Ru nt. The configuration of the ai e entered wake turbulence. Bell 47-G4A cted a takeoff from a truck with r a spraying run in the opposite nce and began to settle, and the re did not operate because of Champion 7ECA e and circling a farm that belon king for a field in which to land | e pilot began practicing instru- nway 28, following a British / rplane indicated that the pilot substantial winds from the northeast at for e direction. He was unaware o he pilot increased collective to corrosion from chemicals car destroyed ged to the pilot's sister. After twa and that on the second pass, t | Arospace BAe 146. A witnes the may have been conducting 1 uninjured our knots to six knots. He flew a f the wind shift to the northwes stop the descent. He attempte ried on the previous flight. 2 serious to passes, the airplane struck the the airplane was flown into wak |
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Location Date Aircraft Type Aircraft Damage Injuries May 31, 1987 Santa Ana, California Gulfstream AA-5B 2 uninjured none The airplane was flown into wake turbulence during takeoff and settled back on the runway. The airplane then veered off the runway into dirt. May 22, 1987 Newport, Arkansas Grumman G164 substantial 1 minor The pilot was conducting an agricultural-operations flight in a rice field in formation with another airplane when his airplane experienced an in-flight upset because of wake turbulence from the other aircraft. The landing gear struck a rice levee and was sheared off. The airplane bounced from a levee and nosed over after striking the ground. April 22, 1987 Richmond, Virginia Cessna 172A minor none* The pilot was conducting a downwind landing when the airplane was flown into wake turbulence from an airliner. The right wingtip contacted the ground, causing minor damage. March 4, 1987 Piper PA-34-200 Miami, Florida substantial 3 uniniured The pilot was flying the airplane on final approach and received ATC clearance to land long when a B-737 was cleared for immediate takeoff. The pilot slowed the airplane for landing, and the airplane was 10 feet AGL to 20 feet AGL when it was flown into wake turbulence, rolled 60 degrees to 70 degrees right and nosed down. The pilot recovered the aircraft to a level attitude and landed on grass to the right of the runway. Radar data indicated that adequate spacing existed between the departing B-737 and the accident airplane. Cessna 170B Feb. 2. 1987 Plaster City, California substantial 2 serious The pilot was flying the airplane about 50 feet AGL at a slow speed with 30 degrees of flaps extended to allow a passenger to photograph a motorcyclist. After completing a 360-degree turn, the airplane was flown through its wake turbulence, stalled and lost altitude. The pilot added power and retracted the flaps. The airplane struck the ground. Dec. 28, 1986 Chicago, Illinois MD DC-9 minor none* During touchdown, the airplane was flown into wake turbulence, and a landing light was damaged. Dec. 19, 1986 Kansas City, Missouri 114 uninjured Boeing 727 minor The aircraft was flown into wake turbulence from a B-747 at FL 310 and received minor damage. Nov. 6, 1986 Tampa, Florida Cessna 421C substantial 4 uninjured The flight crew received clearance for a visual approach behind an L-1011 and was warned of possible wake turbulence. The airplane was flown into wake turbulence at 1,600 feet AGL, and the crew lost control of the airplane, which rolled inverted. The crew performed a "split S" maneuver, regained control of the airplane at 400 feet AGL and landed the airplane. Radar data showed that the L-1011 had crossed the point of the wake-turbulence occurrence 94 seconds earlier at 2,100 feet. Oct. 31, 1986 Fort Pierce, Florida Piper PA-28-181 substantial 2 uninjured The pilot of a U.S. Coast Guard helicopter said on the Unicom frequency that he planned to land the helicopter on Runway 04, then offered to allow the airplane pilot to land the airplane first. The airplane pilot declined. The airplane pilot said later that he observed the helicopter over the runway about 0.5 nautical mile (0.9 kilometer) ahead of his airplane and that he had considered going around, but did not because the air was smooth. During the landing flare, the pilot lost control of the airplane. England Air Force Base, Louisiana Cessna 182 Oct 29 1986 substantial 2 uniniured The airplane was being flown on approach behind four jet fighters. The pilot said that about 200 feet past the runway threshold, at 80 miles (129 kilometers) per hour and three feet AGL, the airplane suddenly touched down on the main landing gear. It then bounced between the main landing gear and the nose landing gear about three times, damaging tips of the propeller blades and the firewall. Oct. 17, 1986 King Salmon, Alaska Piper PA-18-150 substantial 1 minor, 1 uninjured The pilot was cleared to taxi his airplane into position on the runway and to hold behind a Cherokee Six. After the Cherokee Six's departure, the pilot of the accident airplane was cleared for takeoff. Immediately after liftoff, at 10 feet AGL to 15 feet AGL, the airplane entered an uncontrollable right roll. The right wing struck the runway, and the airplane cartwheeled. Sept. 25, 1986 Anchorage, Alaska Starduster SA-100 destroyed 1 serious Shortly after departure of a B-747, the pilot of the experimental airplane was cleared for takeoff. At 200 feet, the pilot lost directional control. and the airplane struck the ground next to the runway. Before takeoff, the pilot had been issued a wake-turbulence advisory. Aug. 30, 1986 Rome, Georgia Midget Mustang M-1 substantial 1 uninjured The pilot conducted a takeoff behind a preceding aircraft, and the airplane was flown into wake turbulence. The turbulence and the left crosswind resulted in loss of control of the airplane, which struck the ground. June 22, 1986 Truckee, California North American AT-6D substantial 2 uninjured During an air show, pilots of three North American AT-6 airplanes conducted takeoffs in what the pilot of the third airplane described as a staggered sequence. The first two airplanes gained altitude without any reported difficulty. The third airplane climbed about 25 feet and was flown into wake turbulence. The airplane violently rolled right and then left. The pilot lost control of the airplane, which struck the runway.

| Date | Location | Aircraft Type | Aircraft Damage | Injuries |
|--|--|---|---|--|
| May 17, 1986 | Van Nuys, California | Socata TB-20 | destroyed | 1 fatal |
| approaching Run | irplane in the traffic pattern for Reway 16R. The pilot said that he sa t 0.25 nautical mile north of the ai | aw the C-130, which was abo | ve his airplane and subsequer | ntly was landed. When the ligh |
| March 31, 1986 | Boise, Idaho | Cessna 210 | substantial | 1 uninjured |
| | are of a transport aircraft being op nce, rolled and struck the ground | | | |
| March 14, 1986 | Bozeman, Montana | Cessna 185 | substantial | 1 uninjured |
| | the airplane's right wing rose, the cting landings on the runway befo | - | 0 | zer struck the ground. A B-76 |
| Jan. 27, 1986 | Reno, Nevada | Cessna 182 | destroyed | 1 fatal |
| wice confirmed t | airplane toward the airport on a V hat he saw the airplane. Witness ound while close behind the B-73 | es said that the accident airp | | |
| Jan. 15, 1986 | Bermuda Dunes, California | Cessna 210E | minor | 1 uninjured |
| Before touchdow | n, the airplane was flown into stror | ng wake turbulence. The airpla | ane rolled and struck the runwa | y hard, damaging the propelle |
| Dec. 19, 1985 | Tucson, Arizona | Cessna 150 | substantial | 1 serious, 1 minor |
| which was appro clearance as the (| wait for departure, the pilot was tolo aching for a touch-and-go landin C-130 passed his airplane's positio The airplane pitched down, rolled i | g. The pilot waived the time on. The accident airplane climb | interval for wake-turbulence s bed to between 25 feet AGL and | eparation and received taked d 50 feet AGL, where it entere |
| Oct. 12, 1985 | Lebanon, Oregon | Cessna 172 | substantial | 1 uninjured |
| • | trol of the airplane during the land nway had generated enough wak | a 1 | | over. A helicopter hovering le |
| Sept. 25, 1985 | Reno, Nevada | Piper PA-22-135 | minor | 1 uninjured |
| After being cautic and the airplane | oned about wake turbulence, the p ground-looped. | bilot began to conduct a taked | off roll. The pilot was unable to | keep the airplane's nose dow |
| Aug. 23, 1985 | Alaska (no further information) | Piper PA-18-150 | none | none* |
| The airplane ente | ered wake turbulence from the lea | ading aircraft during a tander | n takeoff. | |
| Aug. 22, 1985 | Rangely, Colorado | Cessna 172RG | minor | 1 uninjured |
| The airplane tou | ched down short of the runway af | ter being flown into wake tur | bulence from a Beech King Ai | ir. |
| July 25, 1985 | Bonita, Louisiana | Air Tractor AT-301 | substantial | 1 uninjured |
| | ng the second of two aircraft in a ane touched down in a bean field | | rplane was flown into severe v | wake turbulence from the othe |
| July 10, 1985 | Rochester, Minnesota | Cessna 152 | substantial | 1 uninjured |
| | t pilot was preparing to land the a departing DC-9. During the land | | | |
| July 4, 1985 | Dixon, Illinois | North American AT-6 | G substantial | 1 minor, 1 uninjured |
| The pilot conducting the pilot conduction in the conduct the condu | ted a touch-and-go landing behin he ground. | d another aircraft. When the | airplane was four feet to five t | feet above the runway, it rolle |
| June 13, 1985 | Las Vegas, Nevada | Cessna 172 | substantial | 1 minor, 2 uninjured |
| veered right, ther | ng rollout on Runway 19R, with the n departed the runway to the left. d heavy aircraft as weighing more | ATC had cautioned the pilot a | bout wake turbulence from de | |
| June 11, 1985 | Belmar, New Jersey | Cessna 152 | destroyed | 1 fatal, 1 serious |
| During takeoff-ar axiway near Rur | nd-landing practice for a pre-solo f nway 03. The airplane lifted off th aid that the airplane entered the | e runway after a touch-and-g | a helicopter approach the airp to landing, veered right and co | port and hover near the parall |

Location Aircraft Damage Date Aircraft Type Injuries May 3, 1985 Fort Wayne, Indiana Cessna 172P none* minor The pilot lost directional control during takeoff after the airplane was flown into wake turbulence. The aircraft struck VASI lights. March 13, 1985 Dallas, Texas Beech 36 none 3 uniniured The pilot was vectored for an ILS approach to Runway 17L while a B-747 was vectored for an ILS approach to Runway 18R. ATC said that the Beech was at least three nautical miles (5.6 kilometers) behind the B-747, which was descending as it was flown toward the runway from the west. Radar data showed that ATC delayed the B-747's vector to the Runway 18R localizer and that the B-747 flew past the localizer and within 600 feet of the Runway 17L localizer. Wingtip vortices from the B-747 settled at a rate of 400 feet per minute (fpm) to 600 fpm and drifted toward the Beech's flight path. Feb. 28, 1985 West Palm Beach, Florida Piper PA-32 substantial 1 minor, 3 uninjured The pilot radioed approach control to request flight-following services. The controller acknowledged the request and told the pilot to continue flying VFR. The controller asked whether the pilot would keep the airplane below 1,000 feet but did not assign an altitude. The pilot descended the airplane from 1,500 feet to 700 feet, flying south. The controller then told the pilot about heavy jet traffic at his one o'clock position 1.5 nautical miles away, heading west. About one minute later, the airplane was flown into wake turbulence. The pilot completed the flight and subsequently flew the airplane to another airport, where an inspection revealed wrinkled skin on the airplane's wings, popped rivets and firewall deformation. Feb. 19, 1985 Holmwood, Louisiana Boeing A75N1 substantial 1 minor The airplane was one of two that were being repositioned. En route, the airplanes were flown into dense fog, and the pilot of the leading airplane began a 180-degree turn. The second airplane was about 100 feet behind the leading airplane at about 150 feet AGL. While turning, the airplane was flown into wake turbulence from the first airplane, entered a vertical left bank, descended and struck the ground. Oct. 13, 1984 1 uninjured Miles City, Florida Piper PA-J3-C65 destroyed The airplane became uncontrollable after takeoff when it was flown through wake turbulence generated by a departing helicopter, then struck a tree and the ground. Oct. 4, 1984 Norfolk, Virginia Cessna 172 substantial 1 serious The pilot was flying an approach behind a B-727. ATC asked the pilot to fly a short approach and cautioned him about wake turbulence. On final approach at about 50 feet AGL, the airplane rolled sharply into a 90-degree bank, began to roll out of the bank, stalled and turned right about 120 degrees before striking the ground. De Havilland DHC-6-300 Sept. 29, 1984 Houston, Texas minor none* Wake turbulence from a B-727 landing on a parallel runway caused the de Havilland to veer off the side of the runway. The crew was not warned by ATC about wake turbulence. July 18, 1984 Grumman G164-A Stanford, Arkansas substantial 1 minor The pilot flew the agricultural-operations airplane over a set of wires, then, returning across the field, beneath the wires. The airplane was flown through its own wake turbulence and rolled. A wingtip struck the wire. June 30, 1984 Grenada, Mississippi Cessna 172 substantial 1 minor The pilot flew an approach to an uncontrolled airport following 0.25 nautical mile behind a Bell UH-1 helicopter. While on final approach at about 200 feet, the Cessna was flown into severe wake turbulence and rolled nearly inverted. The Cessna struck the ground about 500 feet short of the runway. The pilot said that he was not aware that helicopters produce wake turbulence. June 21, 1984 Middletown, Pennsylvania Cessna 150M destroyed 1 uninjured An airplane flown by a solo student pilot was approaching the runway for landing when ATC told the pilot to go around because a Shorts 330 was on final. The pilot said that during the go-around, his airplane was flown into wake turbulence, cartwheeled and stopped with its nose buried in the ground. June 18, 1984 Charlotte, North Carolina Piper PA-60-600 minor none* The airplane was flown into wake turbulence during takeoff, resulting in a broken right-main-landing-gear scissors. Canadair CL-600 1 serious* May 16, 1984 Clarksville, Texas minor Cruising at FL 350, the aircraft was flown into wake turbulence from a descending B-767. The resultant upset caused an uncontrolled loss of 11,000 feet in 10 seconds to 15 seconds before the crew was able to recover. An unrestrained passenger was seriously injured. April 14, 1984 Kent. Washington Hughes 369 substantial 1 minor The pilot requested clearance to fly through controlled airspace for a landing at Boeing Field. He was advised of a DC-10 being flown on departure from the Seattle-Tacoma (Washington) International Airport and was cautioned about possible wake turbulence. The DC-10 passed 600 feet above the helicopter with about 1.5 nautical miles of lateral separation. Soon afterward, the helicopter was flown into wake turbulence that caused it to exceed 90 degrees of bank and 90 degrees of nose-down attitude; the engine flamed out. The turbulence continued throughout the ensuing autorotation. The pilot tried to flare for a landing, but the main-rotor blades flexed downward and contacted the tail boom March 19, 1984 Riverton, Wyoming Piper PA-12 substantial 1 uniniured The pilot observed a Convair 580 that was landed ahead of his airplane. The pilot flew his airplane on a normal glide path and planned a landing on the approach end of the runway. On short final approach at 50 feet AGL, the airplane suddenly banked more than 90 degrees left and struck the ground 150 feet (46 meters) short of the runway in a left-wing-low attitude.

| | Location | Aircraft Type | Aircraft Damage | Injuries |
|---|---|--|---|--|
| March 18, 1984 | Atlanta, Georgia | Cessna 172P | substantial | 2 uninjured |
| airplane relatively | ducting an emergency landing be y close behind another aircraft in ruck the ground, and the airplane | the traffic pattern. The airplane | | |
| March 6, 1984 | Santa Ana, California | Cessna T210 M | minor | none* |
| A wake-turbulenc | ce advisory was issued to the pilo | ot during landing. The airplane v | was flown into wake turbule | nce and landed hard. |
| Jan. 10, 1984 | Los Angeles, California | MD DC-9 | none | 4 minor, 29 uninjured |
| The DC-9 was flo | own into wake turbulence from an ind the L-1011 and 800 feet below | L-1011 on approach to Runway | y 24L. The DC-9 was six na | • |
| Dec. 6, 1983 | Barbers Point, Hawaii | Cessna 150 | minor | none* |
| The airplane was | in the landing flare when it enter | red wake turbulence from a dep | parting helicopter. A wingtip | struck the runway. |
| Nov. 5, 1983 | West Palm Beach, Florida | Mooney M20J | minor | none* |
| | ectional control when the airplane | • | | |
| | | | - | - |
| Aug. 20, 1983 | Denver, Colorado flown into wake turbulence during | Mooney M20C | minor nunway after the gear had | 1 uninjured |
| | amaged when they contacted the | • | runway aller the gear hau | been reliacted. The properte |
| July 25, 1983 | Chevenne, Wyoming | Cessna 172RG | minor | none* |
| | he pilot was advised of wake tur | | | |
| 0. | • | | | |
| July 18, 1983 | Calipatria, California | Cessna 188 | substantial | 1 uninjured |
| landed hard. | ted a precautionary landing in a c | cotton field during crop dusting a | after feeling the airplane bu | net during a turn. The airpiar |
| July 13, 1983 | Edgar, Nebraska | Cessna 188 | destroyed | 1 uninjured |
| The pilot of the | agricultural-operations airplane the same field. When the pilot | e was completing a turn whe | n the airplane entered wa | ake turbulence from anoth |
| July 1, 1983 | Billings, Montana | Cessna 172R | minor | none* |
| The pilot was ad control of the airp | vised of wake turbulence generational of wake turbulence generation of the second second second second second s | ted by a departing Douglas B-2 | 26 fire tanker aircraft. The p | ilot began the takeoff and lo |
| June 13, 1983 | Oxford, Connecticut | type not specified | minor | none* |
| | ed the takeoff into turbulence gen | erated by a large U.S. Army heli | copter. The pilot lost control | and the airplane struck terrai |
| I he pilot conduct | | | | |
| · | Boston Massachusetts | Cessna 402 | none | 4 uniniured |
| May 13, 1983 | Boston, Massachusetts prological conditions prevailed w | Cessna 402 hen a Cessna 402 was flown i | none in level flight behind an A3 | 4 uninjured 00 in descent for landing. Th |
| May 13, 1983 Instrument meteo | | hen a Cessna 402 was flown i | n level flight behind an A3 | • |
| May 13, 1983 Instrument meter | orological conditions prevailed w | hen a Cessna 402 was flown i | n level flight behind an A3 | • |
| May 13, 1983 Instrument meter Cessna 402 rolle Feb. 6, 1983 The pilot was adv he said that he s approach, about and to land the a | orological conditions prevailed w d inverted. The pilot regained cor | then a Cessna 402 was flown i ntrol and conducted a normal la Beech 35 at was being landed on Runway ad the wake-turbulence warning 7, his airplane suddenly pitched | n level flight behind an A3 anding. substantial y 29R and was cautioned at g. The pilot said that while up and rolled over. He was | 00 in descent for landing. Th 1 uninjured bout possible wake turbulenc he was flying his airplane o able to continue the approad |
| May 13, 1983 Instrument meter Cessna 402 rolle Feb. 6, 1983 The pilot was adv he said that he s approach, about and to land the a seconds behind t | orological conditions prevailed w d inverted. The pilot regained con Tucson, Arizona vised of the position of a B-727 th saw the B-727 and acknowledge two nautical miles from the B-727 irplane safely. The Beech had cr the larger airplane. | then a Cessna 402 was flown i ntrol and conducted a normal la Beech 35 at was being landed on Runway ed the wake-turbulence warning 7, his airplane suddenly pitched rossed the path of the B-727 at | n level flight behind an A3 anding. substantial y 29R and was cautioned at g. The pilot said that while up and rolled over. He was | 00 in descent for landing. Th 1 uninjured bout possible wake turbulenc he was flying his airplane of able to continue the approace |
| May 13, 1983 Instrument meter Cessna 402 rolle Feb. 6, 1983 The pilot was adv he said that he s approach, about and to land the a seconds behind t | orological conditions prevailed w d inverted. The pilot regained con Tucson, Arizona vised of the position of a B-727 th saw the B-727 and acknowledge two nautical miles from the B-727 irplane safely. The Beech had cr the larger airplane. | then a Cessna 402 was flown i ntrol and conducted a normal la Beech 35 at was being landed on Runway ed the wake-turbulence warning 7, his airplane suddenly pitched rossed the path of the B-727 at | n level flight behind an A3 anding. substantial y 29R and was cautioned at g. The pilot said that while up and rolled over. He was | 00 in descent for landing. Th 1 uninjured bout possible wake turbulence he was flying his airplane of able to continue the approa |
| May 13, 1983 Instrument meter Cessna 402 rolle Feb. 6, 1983 The pilot was adv he said that he s approach, about and to land the a seconds behind t *Some reports d ATR = Avions de | orological conditions prevailed w d inverted. The pilot regained con Tucson, Arizona vised of the position of a B-727 th saw the B-727 and acknowledge two nautical miles from the B-727 irplane safely. The Beech had cr the larger airplane. id not include complete details a transport Regional | then a Cessna 402 was flown i ntrol and conducted a normal la Beech 35 at was being landed on Runway ed the wake-turbulence warning 7, his airplane suddenly pitched rossed the path of the B-727 at | n level flight behind an A3 anding. substantial y 29R and was cautioned at g. The pilot said that while up and rolled over. He was | 00 in descent for landing. Th 1 uninjured bout possible wake turbulence he was flying his airplane of able to continue the approa |
| May 13, 1983 Instrument meter Cessna 402 rolle Feb. 6, 1983 The pilot was adv he said that he s approach, about and to land the a seconds behind t *Some reports d ATR = Avions de DA = Diamond A | orological conditions prevailed w d inverted. The pilot regained con Tucson, Arizona vised of the position of a B-727 th saw the B-727 and acknowledge two nautical miles from the B-727 irplane safely. The Beech had cr the larger airplane. id not include complete details a Transport Regional ircraft Industries | then a Cessna 402 was flown i ntrol and conducted a normal la Beech 35 at was being landed on Runway ed the wake-turbulence warning 7, his airplane suddenly pitched rossed the path of the B-727 at | n level flight behind an A3 anding. substantial y 29R and was cautioned at g. The pilot said that while up and rolled over. He was | 00 in descent for landing. Th 1 uninjured bout possible wake turbulence he was flying his airplane of able to continue the approa |
| May 13, 1983 Instrument meter Cessna 402 rolle Feb. 6, 1983 The pilot was adv he said that he s approach, about and to land the a seconds behind t *Some reports d ATR = Avions de DA = Diamond A IAI = Israel Aircra | orological conditions prevailed w d inverted. The pilot regained con Tucson, Arizona vised of the position of a B-727 th saw the B-727 and acknowledge two nautical miles from the B-727 irplane safely. The Beech had cr the larger airplane. id not include complete details a transport Regional ircraft Industries aft Industries | then a Cessna 402 was flown i ntrol and conducted a normal la Beech 35 at was being landed on Runway ed the wake-turbulence warning 7, his airplane suddenly pitched rossed the path of the B-727 at | n level flight behind an A3 anding. substantial y 29R and was cautioned at g. The pilot said that while up and rolled over. He was | 00 in descent for landing. Th 1 uninjured bout possible wake turbulence he was flying his airplane of able to continue the approa |
| May 13, 1983 Instrument meter Cessna 402 rolle Feb. 6, 1983 The pilot was adv he said that he s approach, about and to land the a seconds behind t *Some reports d ATR = Avions de | orological conditions prevailed w d inverted. The pilot regained con Tucson, Arizona vised of the position of a B-727 th saw the B-727 and acknowledge two nautical miles from the B-727 irplane safely. The Beech had cr the larger airplane. id not include complete details a transport Regional ircraft Industries aft Industries I Douglas | then a Cessna 402 was flown i ntrol and conducted a normal la Beech 35 at was being landed on Runway ed the wake-turbulence warning 7, his airplane suddenly pitched rossed the path of the B-727 at | n level flight behind an A3 anding. substantial y 29R and was cautioned at g. The pilot said that while up and rolled over. He was | 00 in descent for landing. Th 1 uninjured bout possible wake turbulenc he was flying his airplane of able to continue the approad |

Aviation Statistics

Data Show That U.S. Helicopter Accidents Increased in 2000 to 10-year High

The U.S. National Transportation Safety Board said that 231 accidents were recorded in 2000; the 11-year total from 1990 through 2000 was 2,211 accidents.

FSF Editorial Staff

Data from the U.S. National Transportation Safety Board (NTSB) show that 231 helicopter accidents were recorded in the United States in 2000, more than any year since 1990, when 233 accidents were recorded (Table 1, page 49).

Of the 231 accidents, 68.8 percent (159 accidents) involved general aviation helicopter operations, 10.8 percent (25 accidents) involved agricultural operations, 6.9 percent (16 accidents) involved on-demand (formerly known as air taxi)/ commercial operations, and 3.0 percent (seven accidents) involved external-load operations. In 10.4 percent (24 accidents) of the accidents, the category of the operation was unknown.

Of the 231 accident helicopters, 21.2 percent (49 helicopters) had reciprocating engines and 18.6 percent (43 helicopters) had turbine engines; in 59.3 percent (137 accidents), the engine type was unknown. (See footnote in Table 1.)

During the 11-year period, 2,211 accidents were reported. Of that number, 68.0 percent (1,503 accidents) involved general aviation operations, 11.9 percent (264 accidents) involved agricultural operations, 7.4 percent (164 accidents) involved

on-demand/commercial operations, and 6.6 percent (146 accidents) involved external-load operations. In 6.1 percent (134 accidents) of the flights, the category of the operation was unknown.

Of the 2,211 accident helicopters, 47.0 percent (1,039 helicopters) had reciprocating engines and 40.6 percent (898 helicopters) had turbine engines; in 12.3 percent (272 accidents), the engine type was unknown. (See footnote in Table 1.) The data did not indicate whether the helicopters were single-engine or multi-engine helicopters.

The data show that the leading causal factor for accidents for the 11-year period was collision with trees (Table 2, page 49); 8.1 percent (180 accidents). Other causal factors included "autorotation, performed," 7.5 percent (165 accidents); "rotor, [revolutions per minute] not maintained," 6.5 percent (144 accidents); "terrain condition, none suitable," 5.7 percent (126 accidents); "clearance, not maintained," 5.3 percent (117 accidents); "aircraft control, not maintained," 5.2 percent (114 accidents); and "object, wire, transmission," 4.5 percent (100 accidents).◆

Table 1U.S. Helicopter Accidents by Category of Operation and Engine Type,1 1990–2000

| Year | Total Accidents | General Aviation | Air Taxi/ Commercial | External-load | Agricultural | Operation Unknown | Reciprocating | Turbine | Engine Type Unknown |
|--------------------|--------------------|---------------------|-------------------------|---------------|--------------|----------------------|---------------|---------|---------------------------|
| 1990 | 233 | 145 | 23 | 19 | 27 | 19 | 132 | 99 | 2 |
| 1991 | 198 | 126 | 20 | 9 | 32 | 11 | 122 | 67 | 9 |
| 1992 | 211 | 149 | 16 | 12 | 22 | 12 | 116 | 70 | 25 |
| 1993 | 183 | 119 | 15 | 17 | 25 | 7 | 94 | 76 | 13 |
| 1994 | 220 | 151 | 17 | 16 | 24 | 12 | 100 | 105 | 15 |
| 1995 | 164 | 114 | 10 | 11 | 24 | 5 | 84 | 76 | 4 |
| 1996 | 181 | 125 | 11 | 15 | 21 | 9 | 77 | 98 | 6 |
| 1997 | 174 | 124 | 10 | 15 | 15 | 10 | 82 | 80 | 12 |
| 1998 | 203 | 149 | 11 | 13 | 24 | 6 | 103 | 83 | 17 |
| 1999 | 213 | 142 | 15 | 12 | 25 | 19 | 80 | 101 | 32 |
| 2000 ² | 231 | 159 | 16 | 7 | 25 | 24 | 49 | 43 | 137 |
| Total ² | 2,211 | 1,503 | 164 | 146 | 264 | 134 | 1,039 | 898 | 272 |

¹Data did not indicate whether helicopters were single-engine or multi-engine helicopters.

²Information was not available to categorize two helicopters according to engine type.

Source: U.S. National Transportation Safety Board

Table 2Top 15 Causal Factors for U.S. Helicopter Accidents, 1990–2000

| Causal Factors | Year | | | | | | | | | | | |
|---|------|------|------|------|------|------|------|------|------|------|------|-------|
| | 1990 | 1991 | 1992 | 1993 | 1994 | 1995 | 1996 | 1997 | 1998 | 1999 | 2000 | Total |
| Object, tree(s) | 18 | 18 | 16 | 19 | 22 | 20 | 20 | 10 | 17 | 15 | 5 | 180 |
| Autorotation, performed | 15 | 17 | 14 | 11 | 13 | 12 | 27 | 17 | 20 | 12 | 7 | 165 |
| Reason for occurrence undetermined, no modifier specified | 15 | 17 | 16 | 17 | 25 | 7 | 11 | 18 | 17 | 13 | 5 | 161 |
| Rotor, RPM not maintained | 17 | 16 | 18 | 16 | 15 | 7 | 6 | 18 | 12 | 17 | 2 | 144 |
| Terrain condition, none suitable | 6 | 15 | 10 | 10 | 18 | 12 | 15 | 12 | 19 | 5 | 4 | 126 |
| Clearance, not maintained | 10 | 11 | 5 | 12 | 18 | 15 | 9 | 10 | 16 | 8 | 3 | 117 |
| Aircraft control, not maintained | 10 | 8 | 7 | 7 | 8 | 13 | 12 | 12 | 14 | 18 | 5 | 114 |
| Object, wire, transmission | 13 | 6 | 8 | 15 | 15 | 8 | 9 | 9 | 10 | 6 | 1 | 100 |
| Autorotation, initiated | 4 | 6 | 10 | 5 | 5 | 5 | 11 | 14 | 13 | 9 | 4 | 86 |
| Terrain condition, water | 7 | 11 | 12 | 8 | 14 | 10 | 4 | 6 | 6 | 5 | 1 | 84 |
| Supervision, inadequate | 4 | 8 | 9 | 9 | 7 | 9 | 11 | 10 | 6 | 5 | 1 | 79 |
| Terrain condition, mountainous/hilly | 3 | 6 | 10 | 7 | 14 | 7 | 9 | 8 | 7 | 6 | 1 | 78 |
| Terrain condition, ground | 4 | 9 | 6 | 2 | 5 | 4 | 5 | 5 | 21 | 11 | 6 | 78 |
| Visual lookout, inadequate | 11 | 8 | 10 | 11 | 7 | 4 | 5 | 4 | 5 | 3 | 1 | 69 |
| Weather condition, tail wind | 9 | 4 | 8 | 6 | 5 | 3 | 5 | 11 | 7 | 6 | 2 | 66 |

RPM = Revolutions per minute

Source: U.S. National Transportation Safety Board

Publications Received at FSF Jerry Lederer Aviation Safety Library

Report Says Coordinated Actions Will Be Required to Reduce Delays in Air Travel

A report by the U.S. General Accounting Office includes recommendations to build new airports outside metropolitan areas, increase use of underutilized airports and redistribute air traffic demand within the current system.

FSF Library Staff

Reports

National Airspace System: Long-term Capacity Planning Needed Despite Recent Reduction in Flight Delays. U.S. General Accounting Office (GAO). December 2001. GAO-02-185. 60 pp. Tables, appendixes. Available from GAO.*

The U.S. air transport system, in recent years, has not been able to accommodate efficiently all aircraft attempting to use limited airspace and busy airports. The number of airline flight delays has increased; in 2000, one flight in four was delayed.

The GAO, which conducts research for the U.S. Congress, said that solving the problem of delays requires action by several sectors of the aviation community because no single sector has the authority or the ability to solve the problem.

"The federal government, especially through the Federal Aviation Administration (FAA) and its parent agency, the Department of Transportation (DOT), plays a major role by operating the nation's air traffic control system, distributing federal funding for airports and setting operating standards for commercial aircraft and airports," the report said. "However, the nation's airports are primarily owned and operated by local units of government, so that decisions about such steps as expanding airport capacity are primarily local in nature. The nation's airlines also play a key role. Their business decisions have a strong effect on the volume and routing of flights, the type and size of aircraft used and the degree to which aircraft are upgraded to take advantage of new technology."

Each group has programs, some developed cooperatively and some independently, under way to address flight delays. Many

programs, such as those to add new runways, were incorporated into FAA's Operational Evolution Plan (OEP). The OEP is a 10-year plan for increasing efficiency and capacity, managing delays, and maintaining safety. Through the OEP, FAA coordinates the implementation of new programs and changes to reduce problems involving congestion and delays. A major portion of the OEP involves the addition of runways at existing airports. The GAO said that current programs, if successful, could add substantial capacity but would not prevent delays from escalating because airports in major cities would have difficulty building additional runways and would continue to be "choke points" in the nationwide interdependent system.

The GAO said that the OEP is a positive step, but if economic conditions (which were affected by terrorist attacks in September 2001) return to or exceed pre-attack levels, the current plan will be inadequate. GAO recommendations include building new airports outside metropolitan areas, increasing use of underutilized airports near capacity-strained metropolitan airports, managing or redistributing air traffic demand within the current system and developing other modes of intercity travel.

Human Factors Design Guidelines for Multifunction Displays. Mejdal, S.; McCauley, M.E.; Beringer, D.B. U.S. Federal Aviation Administration (FAA) Office of Aerospace Medicine (OAM). DOT/FAA/AM-01/17. October 2001. 77 pp. Figures, references. Available through NTIS.**

This report was developed to provide background information and guidelines for FAA safety inspectors who approve multifunction displays (MFDs) for aircraft flight decks. Information in the report also may be useful to those who design such displays.

The report begins with a history of flight deck displays and an explanation of terminology, including a definition of an MFD as "a display surface [that], through hardware [controlling means] or software controlling means, is capable of displaying information from multiple sources and, potentially, in several different reference frames."

MFDs are capable of layering information in integrated formats and using single display surfaces to present large amounts of information from several independent data sources. MFDs are becoming more prevalent in aviation, and there is a need for the same type of guidance for them that already exists for unifunctional displays in the form of guidelines and standards.

The report says that human factors issues arise when avionics components are designed independently, without user input. With an emphasis on human factors design, the report summarizes guidelines by type of display (air traffic, weather, navigation and others). Each section begins with background information and a general description of a type of display or automation process and includes recommended guidelines, limitations and key references from industry literature.

Books

Air Rage: Crisis in the Skies. Anonymous; Thomas, A.R. Amherst, New York, U.S.: Prometheus Books, 2001. 272 pp. Tables, appendixes.

The authors say that air rage, which they define as abnormal, aberrant and abusive behavior by some airline passengers, is the greatest threat to the safety and security of those who fly. The number of air-rage incidents is unknown because of underreporting.

To help readers understand the scope of the problem, the authors identify and discuss fundamental causes of air rage: lack of definition of air rage; a "broken" air transport system; alcohol abuse; drug transport and abuse; smoking prohibition; crowded seating conditions; confusion about carry-on baggage; deported illegal immigrants as passengers; inaccurate and inconsistent reporting of air-rage incidents; and the lack of consequences or penalties for air-rage offenders.

Air Rage: The Underestimated Safety Risk. Dahlberg, A. Aldershot, England: Ashgate Publishing, 2001. 272 pp. Figures, tables, appendixes, bibliography.

The author describes air rage as "a form of workplace violence" and says that the issue has not been acknowledged fully and has not been researched properly. She says that air rage is a system issue and that air travelers are an integral part of the aviation safety system.

One chapter discusses the concept that passengers are a part of human factors in aviation and contains models to help airline personnel focus on service and prevent conflict. The book also discusses adversarial relationships between travelers and aviation employees, with an emphasis on communication and relationships. Another chapter discusses models for airline executives to use in analyzing and developing preventive measures for passenger risk management.

Regulatory Materials

Training, Qualification and Certification of Nondestructive Inspection (NDI) Personnel. U.S. Federal Aviation Administration (FAA) Advisory Circular (AC) 65-31. Oct. 1, 2001. 10 pp. Table. Available from GPO.***

FAA defines nondestructive testing as "inspections, tests or evaluations which may be applied to a structure or component to determine its integrity, composition, electrical or thermal properties, or dimensions without causing a change in any of these characteristics." Performance of such tests and interpretation of test results must be accomplished by trained personnel. Special skills and knowledge of appropriate technical principles and nondestructive testing methods are required.

This AC offers recommendations and criteria for experience, training, qualifying, examining and certifying of testing personnel who inspect aircraft, engines, propellers, accessories and components. This AC may be of interest to testing personnel and those who provide training and supervision of NDI personnel. The AC says that organizations should have a written program that describes guidelines used in training, qualifying and certifying personnel. Inspection personnel who qualify under this AC may be eligible for FAA certification.

Sources

- * U.S. General Accounting Office (GAO) P.O. Box 37050 Washington, DC 20013 U.S. Internet: http://www.gao.gov
- ** National Technical Information Service (NTIS) 5285 Port Royal Road Springfield, VA 22161 U.S. Internet: <http://www.ntis.org>
- *** Superintendent of Documents U.S. Government Printing Office (GPO) Washington, DC 20402 U.S. Internet: http://www.access.gpo.gov>

Accident/Incident Briefs

A340 Crew Conducts Takeoff From Airport Taxiway

The incident report says that the flight crew was cleared for takeoff on Runway 32; instead, they conducted the takeoff on a taxiway nearly perpendicular to the runway.

FSF Editorial Staff

The following information provides an awareness of problems through which such occurrences may be prevented in the future. Accident/incident briefs are based on preliminary information from government agencies, aviation organizations, press information and other sources. This information may not be entirely accurate.



Controllers Saw Airplane's Movement But Did Not Tell Crew to Halt Takeoff

Airbus A340-300. No damage. No injuries.

Night visual meteorological conditions prevailed for the airplane's departure from an airport in the United States for a flight to Taiwan. The flight crew taxied the airplane from the north terminal gate area to Runway 32. They taxied the airplane south on Taxiway Romeo and turned right onto Taxiway Kilo. As the crew made the turn onto Taxiway Kilo — which is nearly perpendicular to the runway — they received clearance from air traffic control (ATC) for takeoff on Runway 32.

"The airplane should have continued west on Kilo to the approach end of Runway 32," the incident report said. "Instead, the airplane accelerated west on Taxiway Kilo."

Both the local controller and a departure controller observed the takeoff roll, but neither controller made a radio call to tell the crew to discontinue the takeoff.

The distance on Taxiway Kilo from the intersection with Taxiway Romeo to the end of Taxiway Kilo is 6,800 feet (2,074 meters). Runway 32 is 11,000 feet (3,355 meters) long. After the takeoff, impressions of main-landing-gear tires were found in a snow bank at the end of Taxiway Kilo.

Landing-gear Shock-strut Door Separates From Airplane

Boeing 767-338. Minor damage. No injuries.

The airplane was being flown at an airspeed below the maximum gear-extension speed of 270 knots on approach to an airport in Australia when the flight crew extended the landing gear. They conducted a normal landing.

Maintenance personnel later told them that the rightmain-landing-gear shock-strut door had separated from the airplane. An examination of the fitting attachments that remained on the door revealed fractures that were "characteristic of rapid overloading," the incident report said.

The report said that the fittings were damaged when the door separated and that they had not contributed to the initial failure.

After the incident, the manufacturer issued an engineering instruction (EI-767-032-0102 Rev 0) to "immediately inspect all B-767 [main-landing-gear] shock-strut doors and check the torque values of the door-attaching hardware." A revision

(EI-767-032-0102 Rev 1) said that the check should be conducted every three months. The report said that the manufacturer developed an engineering change to prevent the main-landing-gear shock-strut-door attach bolts from loosening.

Tail Skid Strikes Runway During Bounced Landing

Boeing 727. Minor damage. No injuries.

The airplane was being vectored for an approach to an airport in England after a flight from Turkey. Because of light turbulence and reports of wind shear, the flight crew increased their approach airspeed by 12 knots to 141 knots.

The airplane crossed the runway threshold at 50 feet and 135 knots. Then, at about 20 feet, the pilot felt the airplane sink rapidly. He raised the nose to a seven-degree or 8-degree noseup attitude, but this had little effect on the rate of descent. The airplane touched down on the main landing gear, then bounced into the air. The pilot raised the nose further, and when the airplane touched down, the tail skid struck the runway. The impact separated the tail-skid plate from the airplane.

The pilot said that the incident was a result of wind shear, an uphill slope on the runway and his insufficient current experience in the airplane type. The report provided no further information on the runway gradient or the pilot's experience.



Icing Blamed for Dual-engine Power Loss

Partenavia P.68B Victor. Substantial damage. Minor injuries.

Night instrument meteorological conditions, with rain and thunderstorms in the area, prevailed for the courier flight in New Zealand.

The pilot flew the airplane to 5,000 feet. She then checked the outside air temperature, which indicated two degrees Celsius (36 degrees Fahrenheit), and used a flashlight to illuminate the wings and engine-air intakes. There was no indication of icing. She conducted the same checks later, after the airplane entered clouds, and again observed no ice.

About 10 minutes after her second check for ice, the pilot observed that the left-engine fuel flow had decreased. An adjustment of the left-engine mixture control restored normal fuel flow, but soon afterward, the problem recurred. The pilot conducted left-engine trouble checks but did not select alternate engine-intake air because she saw no indication of icing.

The pilot told air traffic control about the unexplained power reduction, and then, as she was being given radar vectors, she said that both engines were surging. She shut down the left engine and conducted right-engine trouble checks but did not select alternate engine-intake air because there was no indication of icing. The accident report said that during the approach, the pilot "manipulated the throttle in an attempt to get some power from the engine, but it surged erratically."

The pilot conducted a landing at an en route airport. The airplane overran the runway, struck a fence, crossed a road and struck another fence.

The report said that the engine-air intakes probably became blocked by sleet, ice or hail, which caused the engine problems.

As a result of the accident, the New Zealand Transport Accident Investigation Commission (TAIC) recommended to the New Zealand director of civil aviation that the Partenavia P.68B flight manual be revised to tell pilots to open engine alternateair doors when flying the airplane "in high humidity at any temperature." TAIC recommended to the operator that company pilots be reminded of the Partenavia's "in-flight vulnerability to engine-air-intake blockages by sleet, ice or hail ... and the corrective action necessary should a blockage occur."

The recommendations were accepted.

Loss of Power on Takeoff Prompts Precautionary Landing

Cessna U206G Stationair 6. Minor damage. No injuries.

The airplane was being repositioned after a missionary flight when, at 150 feet above ground level, after takeoff from an airport in Tanzania, the pilot heard a loud popping sound from the engine bay. The pilot observed a slight decrease in power and minor engine roughness, but engine revolutions per minute were unchanged.

The pilot conducted a precautionary landing on the runway and taxied to a parking area in front of the airport fire station.

Inspection revealed that the no. 4 cylinder head had separated from the engine, causing minor damage to adjacent engine parts. The cylinder had been plated about three years earlier and had accumulated 1,015.8 operating hours before the incident. The incident report said that the cylinder baffle between the no. 2 cylinder and the no. 4 cylinder had been replaced the day before the incident; the same repair had been conducted the previous month. A laboratory was conducting metallurgical tests on the no. 4 cylinder.



Fuel-flow Problem Blamed for Uncommanded Engine Shutdown

Canadair CL-600 Challenger. No damage. No injuries.

The airplane was being flown from an airport in Canada on a routine flight inspection of instrument landing system equipment when the flight crew reported an uncommanded shutdown of the right engine (General Electric CF-34-3A1). The crew declared an emergency and landed with the engine inoperative.

An inspection and ground tests of the engine revealed no engine abnormalities. Subsequent analysis of data from the flight data recorder revealed that there had been an interruption of fuel flow to the right engine. The operator was investigating to determine the cause of the fuel-flow interruption.

Airplane Strikes Ground During IFR Departure

Piper PA-32-300 Six 300. Destroyed. Four fatalities.

Instrument meteorological conditions prevailed, and an instrument flight rules flight plan had been filed for the afternoon departure from an airport in the United States.

When air traffic control (ATC) issued the takeoff clearance, the pilot was told that, after takeoff, he should turn the airplane left to a departure heading of 90 degrees. When the pilot called ATC (departure control), he said that the airplane was at 1,500 feet and climbing. ATC told the pilot to fly the airplane to 4,000 feet. Two minutes later, ATC again told the pilot to fly a heading of 90 degrees. The pilot repeated the heading assignment, but radar data show that the airplane was flown in "a wide arc to the right and back over the airport, then [in] a 360-degree turn to the right," the accident report said.

"Departure control again contacted [the pilot] to advise of the 90[-degree] heading, which the pilot acknowledged," the report said. "Departure control then advised the pilot of the apparent

360-degree turn, and the pilot acknowledged. ... Departure control requested [the pilot] to say [his airplane's] present heading, and the pilot reported a heading of 240 degrees. ... Departure control advised [the pilot] that the heading should be 90 degrees, and the pilot acknowledged and asked if that would be a right turn to 90 [degrees]. Departure control replied left turn to 90 [degrees]."

Radar data showed that the airplane was at 4,000 feet in a level turn that resulted in a heading of about 60 degrees. The heading then varied from 45 degrees to 74 degrees before the airplane turned right and descended.

The report said, "Departure control asked the pilot ... what [he] was trying to do. The pilot reported that he was trying to get out of a spin."

One minute later, radar data showed that the airplane turned right and descended to 3,300 feet. Witnesses said that the airplane crossed a highway below clouds, apparently at a level attitude, then turned right and, in a steep, nose-low, right-wing-low attitude, the airplane struck trees.

Airplane Strikes Glacier During Approach in Instrument Conditions

Beech 300LW Super King Air. Destroyed. Two fatalities.

An instrument flight rules (IFR) flight plan had been filed for the flight from Poland to Switzerland, and visual meteorological conditions had prevailed for most of the flight.

The pilot canceled his IFR flight plan and began a visual approach to the airport, which had no instrument approach procedure. Low clouds were reported near the airport at the time of the accident, and the weather 22 nautical miles (41 kilometers) northeast of the accident site included a 2,000-foot overcast and visibility of one-half mile (0.8 kilometer) in fog. The airplane struck a glacier at 9,842 feet.



Interrupted Preflight Check Precedes Takeoff With Tow Bar on Nosewheel

Cessna 310R. Minor damage. No injuries.

A preflight check of the airplane was conducted at midday in the hangar at an airport in England. Later, the airplane was hand-towed by airport employees to the concrete apron outside the hangar. They parked the airplane and left the tow bar attached to the nosewheel.

When the pilot arrived, he began completing preflight checks but was interrupted when his cellular telephone rang. He boarded the airplane to answer his phone and was told that the flight was no longer necessary. Because he planned to start the engines to reposition the airplane in the grass parking area, he decided to fly the airplane in the traffic pattern. He started the engines and taxied to the active runway, using power for directional control, the report said.

When the airplane reached 30 miles (48 kilometers) per hour on the takeoff roll, it turned left. The pilot applied right rudder but could not stop the turn. He moved the throttle levers to idle and applied right brake. The airplane left the runway and rolled into an adjacent field, and the nose landing gear collapsed.

The accident report said that the pilot "had not completed his external check when he got into the aircraft to answer the mobile phone and had not noticed that the tow bar was still attached."

Aircraft Strikes Trees After Takeoff From Runway With Uphill Slope

Piper PA-28-151. Destroyed. No injuries.

Visual meteorological conditions prevailed for the departure from an airport in Sweden. The pilot selected 10 degrees of flaps and conducted a normal takeoff on Runway 25, which is 650 meters (2,133 feet) long with the first portion sloping uphill. Winds were from the southwest at five knots to 10 knots. The pilot said that the acceleration was sluggish and that he checked the foot brakes and the parking brake to ensure that neither was engaged.

"The airplane became airborne a few times but bounced onto the runway again prior to the final liftoff, which took place less than 50 meters [164 feet] from the runway end," the accident report said. "The stall warning was activated during a major portion of the takeoff run."

After about 100 meters (328 feet) of flight, the airplane struck a bush. Flight continued for about 200 meters (656 feet) before the airplane struck trees about three meters to four meters (10 feet to 13 feet) tall.

The report said that "for all practical purposes, the runway was too short, due to the uphill slope," and that the pilot used a "disadvantageous flap setting" and did not conduct a short-field takeoff. The report also said that correction factors for takeoffs from runways with uphill slopes were not included in the aircraft operations manual or in the Swedish Rules of Civil Aviation.

Airplane Strikes Terrain During Simulated Engine Failure

Jabiru ST3. Destroyed. Two fatalities.

Other pilots said that they heard the pilot say on the radio that he was conducting a simulated engine failure during approach to an airport in Australia before the single-engine airplane struck an embankment about 210 meters (689 feet) north of the runway on the extended centerline.

An investigation revealed that the airplane struck terrain in a nose-high, left-wing-low attitude, that the engine was producing power at the time of impact and that the airplane had no known flight control deficiencies. The accident report said that trees next to the airport caused localized turbulence, wind shear and downdrafts when the wind was from the southeast. At the time of the accident, the wind was from 150 degrees at 15 knots, with gusts to 18 knots. The report said that the airplane probably encountered turbulence and a high sink rate generated by the wind over the nearby trees.

"Given the evidence of significant power at the time of impact, it is possible that the pilot had initiated a go-around at a stage in the approach from which it was not possible to establish a positive rate of climb," the report said.



Pilot's Judgment Faulted in Autorotation Accident

Hughes 369E. Substantial damage. No injuries.

Visual meteorological conditions prevailed just before sunset in Sweden when the pilot — who had been on flight duty for 10 hours, had flown the helicopter for four hours and 20 minutes and had conducted 30 takeoffs and landings decided to conduct a training flight that included emergency exercises.

After about 30 minutes of flight, the pilot began to conduct an autorotation and a landing. Because the helicopter's airspeed was high — about 70 knots — the pilot initiated a recovery. The accident report said that the main-rotor revolutions per minute (rpm) were low during touchdown, "and the contact with the ground proved to be hard and took place with a certain amount of forward motion. ... After touchdown, the pilot

noticed an object that came from behind him and passed by diagonally out to the right."

The pilot shut down the engine and observed that the tail boom had been severed by the main rotor.

The report said, "Complete autorotation maneuvers place large demands upon the pilot, and the margins for misjudgment are not large. In this case, the pilot made a miscalculation, which resulted in main-rotor rpm being too low when he initiated the final recovery prior to touchdown. ... Contributory to the occurrence might have been that the pilot was somewhat tired after a long workday."

Mountain Turbulence Cited in Student Pilot's Loss of Control

Agusta-Bell 47G-2A1. Destroyed. One fatality.

Visual meteorological conditions prevailed for the student pilot's solo flight from an airport in Australia. Air traffic control radar tracked the helicopter intermittently for about 40 minutes; the helicopter was last observed on radar about seven nautical miles (13 kilometers) northeast of the accident site.

A witness observed the helicopter being flown "in a manner consistent with the pilot experiencing controllability difficulties," the accident report said. The wreckage was found on a mountain slope about one nautical mile (1.9 kilometers) off the student pilot's planned course. Notes containing preflight navigation planning calculations were found nearby, but the calculations did not take into consideration the forecast winds en route.

"Personnel at the flight-training school did not recall discussing at length the forecast weather conditions with the pilot and, in particular, they did not recall briefing the pilot about the forecast mountain waves prior to the navigation exercise," the report said.

Flight-training personnel said, however, that helicopters had been flown in the area throughout the day and that the pilots had not experienced controllability problems.

The weather forecast for the area, issued about two hours before the accident, was for isolated severe turbulence and mountain waves below 9,000 feet. Subsequent analysis of weather data indicated that at 1,500 feet — the altitude at which the pilot had planned to fly — winds were conducive to mountain waves and rotor. Photographs indicated that the helicopter probably was flown into severe turbulence from

mountain waves or rotor and that the main-rotor blades may have severed the tail boom.

"This accident signature is consistent with excessive blade flapping," the report said. "The evidence indicated that a divergence of the main-rotor blade from its normal plane of rotation probably occurred as a result of severe turbulence generated by mountain wave or rotor activity, and a main-rotor blade contact with the tail boom and cockpit area ensued, resulting in a loss of control of the helicopter.

"It is also possible that the collective lever friction may have been overcome by the severe turbulence that caused the nonpowered collective lever to suddenly drop. The collective lever drop would have induced a sudden nose-down attitude, and this may have caught the pilot by surprise. The pilot may have instinctively and rapidly applied aft cyclic to correct the aircraft's attitude. The rapid application of aft cyclic in this situation may have been sufficient to induce main-rotor blade contact with the tail boom."

Helicopter Strikes Highway, Motor Vehicle in Fog

Robinson R44. Destroyed. One fatality, one serious injury, one minor injury.

The helicopter was being flown to its hangar at an airport in the United States after a photographic flight. The accident report said that "visual to instrument meteorological conditions" prevailed in the area; witnesses described a dark night with fog, clouds and drizzle.

One witness said that he was driving a motor vehicle when he observed a red light about 100 feet above the highway median. He said that fog obscured his vision but that the light rose "almost straight upward another 200 feet and then began corkscrewing downward."

The helicopter struck the highway and one motor vehicle; three other motor vehicles received minor damage. The wreckage was about 200 feet southwest of power lines that cross the highway.

An investigation revealed a tear in the fiberglass portion of the front-right side of the cabin, a scratch on the right-side doors and "semicircular deformation" in the right navigationlight assembly and the tail skid. The crew of a power-linemaintenance helicopter observed a streak on the southwest side of the power lines that contained a red, white and blue material. The helicopter's color scheme was blue, with white and red designs.◆

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